

Statement of Environmental Effects Proposed Installation of a Hail Proof Netting Structure

5721B and 5758 Sturt Highway, Monak

for G2 Netting Group September 2025



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Executive Summary

This Statement of Environmental Effects (SEE) has been prepared by MasterPlan Pty Ltd ('MasterPlan') in support of a development application (DA) made by G2 Netting Group (the 'applicant') seeking a development consent for a proposal to install a hail proof netting structure. The DA is made to the Wentworth Shire Council under the *Environmental Planning and Assessment Act 1979 (NSW)* (EP&A Act) .

The DA is made over land located at 5271B and 5758 Sturt Highway, Monak (the 'Subject Site' or 'Site').

The Site is in RU1 Primary Production Zone of the Wentworth Local Environmental Plan where the proposed development is 'permitted with consent' thereby triggering the need for a development application to be made.

The assessment provided within this report and associated supporting documentation demonstrates that the proposal satisfies the requirements of the relevant planning instruments and represents an appropriate development outcome for the site and its local setting. It is the conclusion of our assessment that there are strong grounds for the Council to approve the application subject to reasonable and relevant conditions.

Site and Proposal Details			
Address of Site	5271B Sturt Highway, Monak		
	5758 Sturt Highway, Monak		
Legal Description	2/-/DP1248259 – Lot 2 in Deposited Plan 1248259 at Monak Local Government Area		
	Wentworth, Parish of Paringi, County of Wentworth		
	2/-/DP827371 – Lot 2 in Deposited Plan 827371 at Monak Local Government Area		
	Wentworth, Parish of Paringi, County of Wentworth		
Site Area	25.42 hectares (ha)		
Easements	Right of Carriageway		
	Pipeline Easements		
	Pump Site Easement		
	(*see Section 2.21 for details)		
Existing Use	Horticultural land comprising vineyards		
Landowner	P & E Marciano Pty Ltd		
Proponent	G2 Netting Group		
Local Government	Wentworth Shire Council		



Site and Proposal Details				
State Environmental Planning Policies	Biodiversity and Conservation			
(SEPP)	Exempt and Complying Development Codes			
	Housing			
	Industry and Employment			
	Planning Systems			
	Primary Production			
	Resilience and Hazards			
	Resources and Energy			
	Sustainable Buildings			
	Transport and Infrastructure			
Local Environmental Plan (LEP)	Wentworth Local Environmental Plan 2011			
Development Control Plan	Wentworth Shire Development Control Plan, December 2011			
Defined Use	Farm Building			
Zone	RU1 – Primary Production			
Category of Development Consent	Permitted with Consent			

Applicant Details				
Applicant	G2 Netting Group			
Applicant's Representative	Jasmine Walters (MasterPlan)			
Applicant's Contact Details	MasterPlan Pty Ltd			
	33 Carrington Street, Adelaide SA 5000			
	(08) 8193 5600			
	jasminew@masterplan.com.au			
MasterPlan Reference	20071			



1 Introduction

1.1 Overview

This Statement of Environmental Effects (SEE) has been prepared by MasterPlan in support of an application made by G2 Netting Group (the 'applicant') seeking a development consent for a proposal to install a hail proof netting structure (HPN). The application is made to the Wentworth Shire Council (the 'Council') under the *Environmental Planning and Assessment Act 1979 (NSW)* (EP&A Act).

MasterPlan delivers urban and regional planning services across Australia through offices in South Australia, the Northern Territory and Queensland. This report has been prepared in MasterPlan's South Australian office.

G2 Netting Group is the proponent of the development. The proposed development for the installation of a hail proof netting (HPN) structure will enable the landowner to continue their existing horticultural activities on the subject land.

The application is made over land located at 5271B Sturt Highway, Monak (the 'Subject Site').

The site is within the RU1 Primary Production Zone of the Wentworth Local Environmental Plan (LEP) where the proposal is 'permitted with consent' thereby triggering the need for a development application.

In accordance with the LEP, the proposed development is defined as a 'farm building', which is permitted with consent in the RU1 Zone. For this purpose, a 'farm building' is defined as:

...a structure the use of which is ancillary to an agricultural use of the landholding on which it is situated and includes a hay shed, stock holding yard, machinery shed, shearing shed, silo, storage tank, outbuilding or the like, but does not include a dwelling.

Applications for development consent are required to be assessed by the Council in accordance with the statutory requirements of the EP&A Act. The purpose of this SEE is to describe the site and its environs, the development and operational details of the proposal, the potential environmental impacts of the proposal, and the steps to be taken to protect the environment or to lessen the expected harm to the environment. This SEE also provides an assessment of the proposal in terms of the matters for consideration under Section 4.15 of the EP&A Act.

1.2 Specialist Consultants

This report should be read in conjunction with plans, drawings, and reports prepared by the following specialist consultants:

• G2 Netting Group – Plans, Elevations and Structural Details



1.3 Pre-Lodgement Engagement with the Council

1.3.1 Communications

Pre-lodgement communications were not conducted with the Council prior to lodging the application

1.3.2 Meetings

A pre-lodgement meeting was not held with the Council prior to lodging the application.

1.4 Pre-Lodgement Engagement with State Government

1.4.1 Communications

Pre-lodgement communications were not conducted with any agency of the NSW State Government prior to lodging the application.

1.4.2 Meetings

Pre-lodgement meetings were not held with any agency of the NSW State Government prior to lodging the application.

1.5 Community Engagement

Engagement was not undertaken with the community prior to lodging the application.



2 Context and Site Information

2.1 Context Information

2.1.1 Location and Land Uses

The subject land is located at 5271B Sturt Highway in the suburb of Monak within in the local government area of the Wentworth Shire Council (the 'Council'). The proposed development comprises three (3) adjoining netting structures which will cover existing vineyards as shown in **Figure 1** below.

Land use patterns within the locality of the subject land are depicted in the Site, Locality and Zone Plan provided in **Appendix A**.

The surrounding uses in the neighbourhood of the Site are described in **Table 1** below.

Table 1: Surrounding Uses

Direction from Site	Surrounding Uses
North	Existing vineyard and ancillary structures including a dwelling
South	Murray River
East	Existing vineyard and ancillary structures including a dwelling
West	Existing vineyard and ancillary structures including a dwelling





Figure 1: Development Site(s) (excerpt from Proposed Site Plan).



2.1.2 Sensitive Land Uses

There are sensitive land uses (i.e., dwellings) located within proximity to the nearest development site as listed in **Table 2** below.

Table 2: Sensitive Land Uses

Land Use	Likely Sensitivity	Proximity to Site	Direction from Site
Dwelling	Visual	12 m	South-east
Dwelling	Visual	67m	South-east
Dwelling	Visual	64m	South-east
Dwelling	Visual	112m	South-east
Dwelling	Visual	190m	North-west
Dwelling	Visual	254m	North-west
Dwelling	Visual	533m	North-east
Dwelling	Visual	40m	West
Dwelling	Visual	650m	West

2.1.3 Topographical Context

The land is relatively flat, with a gentle fall from north-west to south-east where the land meets the Murray River. The development comprises netting roof and walls which allows for sunlight penetration. Larger trees along the northern site boundary and adjacent the on-site dwellings will not be materially shaded by the proposed structures.

2.1.4 Transport Networks

The subject land is accessed via Sturt Highway which is a State Highway that extends across the New South Wales, Victorian and South Australian State boundaries.

Within proximity of the subject land, Sturt Highway operates as a two-lane bi-directional road which is sealed without kerbing. The road shoulder is approximately 19m on the northern side of the road and 16m on the southern side. The Highway is an important freight route for the region, and as such, the road is designed to accommodate large vehicles including B-Doubles.



2.1.5 Community Facilities

The townships of Gol Gol and Buronga are nearest the site, being located approximately 13 kilometres north-east of the subject land. These townships include a number of community facilities including supermarkets, hotels, child care centres and recreation facilities.

Approximately 2 kilometres further north-east, on the southern side of the Murray River, is the much larger township of Mildura, Victoria. With a population of some 35,000 persons, this township is equipped to provide a full catalogue of community facilities within the region. Mildura offers a range of medical services including a hospital, a range of recreation facilities, civic facilities including public libraries and museums, educational facilities, and other community facilities including halls, churches and community centres.

2.1.6 Neighbourhood Character

The neighbourhood character is best described as rural farm land with a number of vineyards being prevalent within the immediate locality of the subject land. There are also vast expanses of untouched scrubland within the broader locality, particularly north and east of the subject land.

Riparian land is evident south of the subject land bordering the Murray River.

2.2 Site Information

2.2.1 Title and Survey Details

The Site Plan provided in **Appendix B** depicts land parcel boundaries, land parcels boundaries, road parcels, and easements on the site of the proposed development.

The site comprises one (1) allotment with an area of 25.42 hectares and is held under freehold title by the registered owners of the site as outlined in **Table 3** below.

Table 3: Site Details

Address	Lot And Plan	Lot Area	Owner
5721B Sturt Highway, Monak	Lot 2 in Deposited Plan 1248259	25.42 hectares	P & E Marciano Pty Ltd
5758	Lot 2 in Deposited Plan 827371	20 hectares approximately	P & E Marciano Pty Ltd

Any minerals found on the land are the property of the Crown. In addition, the property is subject to the easements and rights of carriageway described in **Table 4** below.



Table 4: Easements

Easement / Right of Carriageway	Width	Purpose
Right of Carriageway	4 metres	Vehicle access
Right of Carriageway	6 metres	Vehicle access
Easement	6 metres	Pipeline
Easement	3 metres	Pipeline
Easement	6 metres	Pipeline
Easement	9.4 metres	Pump Site

Search copies of Certificates of Title and Survey Plans for the Site are provided in **Appendix C**.

2.2.2 Historical Use

We understand from aerial imagery that the subject land has been used for agricultural purposes, including grazing and cropping activities, since prior to 2002.

2.2.3 Existing Development

The subject land is currently improved by the following:

- Five (5) residential dwellings
- Farm buildings (i.e., hay sheds and outbuildings)

The land in its current form is depicted in the Site Plan contained in **Appendix A**.

2.2.4 Road Access

The site has a primary frontage to Sturt Highway of approximately 186.34 metres with two (2) existing crossovers. The land also has rights of carriageway over the adjoining allotments to the east and west, as well as a right of carriageway across the adjoining allotments from Bonnie Doon Road.

The site also comprises internal tracks within the site boundaries, to allow for vehicular and equipment movement around the site.

2.2.5 Car Parking and Loading

All car parking is located on-site, with formal parking areas located within close proximity to each of the dwellings.

Farm equipment is stored near or within the existing farm buildings.



2.2.6 Fencing

There is no existing boundary fencing evident around the site.

2.2.7 Utilities and Services

Dial Before You Dig records of services infrastructure for the site indicate that it is connected to the reticulated urban electrical and telecommunications infrastructure.

Existing electrical infrastructure for the site runs overhead between posts. We note that there are no high-tension poles located on the subject land.

The site does not have access to reticulated urban sewer or water.

Maps obtained from the Dial Before You Dig service for the site are shown in **Appendix D**.

An Infrastructure Agreement is not applicable to the site.

2.2.8 Landscape Features

The land consists primarily of vineyards with four (4) distinctive crops visible from aerial imagery. Some localised landscaping exists in and around the dwellings located on the site. A row of trees is evident along the primary frontage to Sturt Highway.

Wetlands are evident in the southern portion of the site, with riparian land evident where the land directly adjoins the Murray River.

2.2.9 Topography

The land gently falls from north-west to south-east where the land meets the Murray River.

2.2.10 Terrestrial Biodiversity

The site is identified as containing Terrestrial Biodiversity land consisting of the wetlands and riparian land adjacent the Murray River, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer (refer **Appendix E**).

2.2.11 Groundwater Vulnerability

The site is not identified as being in a Groundwater Vulnerability Area as indicated on the maps provided in the State Government's ePlanning Spatial Viewer. The adjacent Murray River is identified as being in a Groundwater Vulnerability Area and is further identified as Environmentally Sensitive Land.



2.2.12 Riparian Lands and Watercourses

The site is identified as being in a Riparian Lands and Watercourses Area with Natural Resources Sensitivity – Watercourse, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer (refer **Appendix F**).

2.2.13 Wetlands

Wetlands are identified on the site as indicated on the maps provided in the State Government's ePlanning Spatial Viewer (refer **Appendix G**).

2.2.14 Environmentally Sensitive Land

The site is not identified as containing environmentally sensitive land, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.15 Scenic Protection

The site is not identified as containing scenic protection land, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.16 Airport Noise and Obstacle Limitation Surface

The site is not identified as being in an Airport Noise Area or as being impacted by an Obstacle Limitation Surface, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer

2.2.17 Salinity

The site is not identified as having potential salinity issues, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.18 Flood Hazards

The site is not identified as being in a Flood Planning Area, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.19 Bush Fire Hazards

The site is identified as partially containing bush fire prone land Vegetation Category 1, with a Vegetation buffer to the north, as indicated on the maps provided in the State Government's ePlanning Spatial Viewer (refer **Appendix H**).



2.2.20 Contaminated Land

A search of the Contaminated Sites Database and the Reported Sites Register indicates that the site does not contain known or suspected contaminated sites.

2.2.21 Acid Sulfate Soils

The site is not identified as containing potential acid sulfate soils as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.22 Heritage, Cultural and Archaeological Values

Dareton is the Local Aboriginal Land Council for the locality.

A search of the Aboriginal Heritage Information Management System (AHIMS) indicates that there are no records or information about Aboriginal places, objects and other significant sites that affect the site (refer **Appendix I**).

The site has no known non-indigenous heritage values.

2.2.23 Mineral and Resource Land

The site is not identified as being Mineral and Resource Land as indicated on the maps provided in the State Government's ePlanning Spatial Viewer.

2.2.24 Minerals and Resources Permits

There are no current exploration or production permits on or surrounding the site.

There is evidence of a historic licence (EL5510) held between 2000 and 2004.

2.2.25 Extractive Resources

There are no extractive resource operations on or surrounding the site.

2.3 Development Approval History

A search of the NSW Planning Portal Application Tracker identifies that no recent development permits have been issued for the site.



3 Proposal

3.1 Proposal Overview

In consideration of Section 1.5(1) of the EP&A Act the proposed development comprises:

1. The erection of three (3) adjoining farm buildings comprising Hail Protective Netting Structures and ancillary posts and anchors.

Development of the site is proposed to occur in a single stage.

The proposed structures will be located over the existing vineyards contained in the north-east and south-western portions of the land, excluding those areas comprising overhead powerlines, dwellings and other ancillary structures.

3.2 Plans of Development

The Proposal is depicted on the Plans of Development listed in **Table 5** below and provided in **Appendix B**.

Table 5: Proposed Details

Plan / Drawing No.	Prepared By	Drawing Title	Date Of Issue
Project No. 1759, Sheet 101A	G2 Netting Group	Existing Site Plan	30 June 2025
Project No. 1759, Sheet 102	G2 Netting Group	Proposed Site Plan	30 June 2025
Project No. 1759, Sheet 001	G2 Netting Group	Site – Plan	30 June 2025
Project No. 1759, Sheet 002	G2 Netting Group	Detail Sheet 01	30 June 2025
1759-CR01 _P&T_ Marciano_ FlatTop_ Structural _ Evaluation_27May25	G2 Netting Group	FLAT TOP Structure Evaluation Spreadsheet V2024-09 [Engineering Specifications]	27 May 2025

3.3 Works Aspects

3.3.1 Construction Works

The proposed development incorporates the construction of hail protective netting (HPN) structures, including ancillary posts, anchors and side netting. The location, scale and form of the proposed structures are summarised in **Table 6**.



Table 6: Key Design Parameters

Building/Structure	Location on Site	Key Design Parameter	Dimensions
HPN 1	South-western portion of the site	Minimum setbacks to boundaries	1m western site boundary
	within proximity of the western site boundary.	Maximum building height	5m above natural ground level
		Roof dimensions / area	214.4m (w) x 229.8m (l) Area = 41,497m ²
HPN 2	North-eastern portion of the site within proximity of the eastern site boundary.	Minimum setbacks to boundaries	8.6m southern site boundary 2.3m – 5.1m eastern site boundary
		Maximum building height	5m above natural ground level
		Roof dimensions / area	214.4m (w) x 216.6m (l) Area = 48,314m ²
HPN 3	North-eastern portion of the site within proximity of the north and east site boundaries.	Minimum setbacks to boundaries	30m eastern site boundary 0.5m northern site boundary
	east site boundaries.	Maximum building height	5m above natural ground level
		Roof dimensions / area	246m (w) x 293.2m (l) Area = 73,486m ²

The total site coverage of the proposed buildings is 163,297m2 (16.3ha) or 64.2% of the site. We note however that the structure is permeable and is covering existing vineyards.

3.3.2 Construction Materials and Colour Schemes

The construction materials and colour schemes of the proposed buildings are summarised in **Table 7**.

Table 7: Construction Materials and Exterior Decorations

Building	Building Component	Construction Materials	Colour Schemes
HPN Structures (*Note - each structure	Top Netting	Lock stitch knitted HDPE monofilament yarn (20mm hexagonal hole)	White
will comprise the same Construction materials and colour scheme)	Side Netting	Lock stitch knitted HDPE monofilament yarn (16-20mm hexagonal hole)	Black
	Posts	Corners – Stainless steel Perimeter – tubular steel Internal – steel Internal breaker – iron bark (timber) Perimeter breaker – steel post base	



Building	Building Component	Construction Materials	Colour Schemes
	Wire and Cables	Galvanised steel	n/a
	Post Footings	Cast-in-Place Concrete	n/a

The buildings proposed to be constructed as part of the development of the site are depicted on the Plans of Development provided in **Appendix B**.

3.3.3 Methods of Construction and Site Management

Netting Structures 1, 2 and 3 will be constructed on-site.

The construction site will be managed to ensure to protect the health, safety and welfare of workers and other people in accordance with the NSW work health and safety legal framework as set out under the:

- Work Health and Safety Act 2011
- Work Health and Safety Regulation 2017
- Relevant Codes of Practice.

3.3.4 Excavation and Fill

The proponent has confirmed that the proposed development will include post holes of no greater depth than 600 millimetres (mm) to support the HPN structures.

3.3.5 Construction Traffic

The proposed development is anticipated to generate minimal traffic movements associated with:

- Construction materials being delivered to the site.
- Installation specialists being on-site during construction.

The number and frequency of truck movements will be minimal and largely contained within the site boundaries.

The direction of vehicle and truck movements on the adjacent local road network will be in an east/west direction, travelling to/from Mildura to the development site via Sturt Highway.

3.3.6 Services and Infrastructure

It is not anticipated that any site services will be impacted by the proposed building works. Electrical cables servicing the site are generally located above ground and do not encroach on the development site.



The proposal comprises minimal ground works, other than to secure posts and anchors. The Dial Before You Dig Australia service will be utilised to identify any potential conflicts with underground services.

3.3.7 Vegetation Clearance

With the exception of the vineyards, the site of the proposed HPN structures is relatively devoid of vegetation. Localised landscaping exists around the on-site dwellings and a row of trees along the site's frontage to Sturt Highway is also evident. The southern-most portion of the site comprises native vegetation.

The proposed development will not involve the removal, destruction or lopping of trees and the removal of vegetation.

3.3.8 Landscaping

The proposed development will not involve any landscape works.

3.4 Construction Impacts

3.4.1 Noise Impacts

The proposed construction of the development is not anticipated to generate any significant increase in noise generation above existing levels, particularly those experienced by farm equipment and vehicle movements on Sturt Highway.

3.4.2 Traffic Impacts

The construction of the proposed development is not anticipated to generate any significant increase in traffic generation to/from the site above existing levels and the construction period will be relatively short in duration.



4 Planning Controls and Permit Triggers

The requirement to obtain approval prior to the commencement or carrying out of development is derived from Part 4 of the EP&A Act. The relevant State Environmental Planning Policies (SEPPs) and Local Environmental Plans (LEPs) outline when development approval is required or not required.

4.1 Mapped Planning Controls

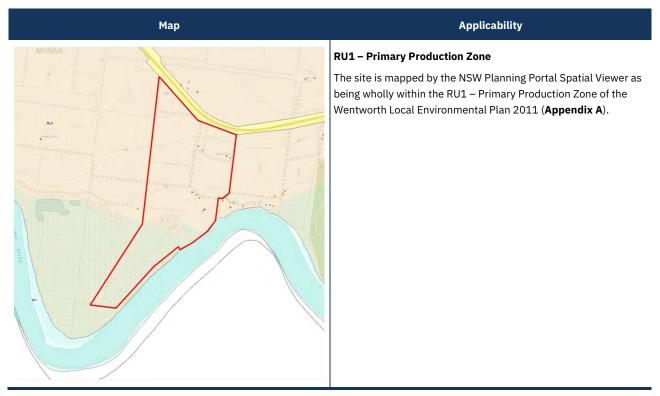
4.1.1 Property Report

A copy of the Property Report for the site obtained from the State Government's Planning Database is provided in **Appendix J**.

4.1.2 Planning Controls

Under the LEP, the Site is subject to planning controls that apply to the whole or parts of the Site as depicted in **Table 8**.

Table 8: Planning Controls





Map Applicability



Riparian Lands and Watercourses.

The site is identified as being affected by a Watercourse, namely the Murray River which runs adjacent the southern site boundary (**Appendix F**).

Notwithstanding, the site of the proposed structures is not located within the portion of affected land and will be setback approximately 60 metres from the watercourse.



Terrestrial Biodiversity

The site is identified as comprising some land of Terrestrial Biodiversity (**Appendix E**).

The land identified predominantly affects the southern-most portion of the land and the land adjacent the Murray River. A small portion of land along the southern edge of HPN 1 is located within the Terrestrial Biodiversity overlay. Notwithstanding, the land appears to have already been compromised by historical agricultural practices occurring on the land.



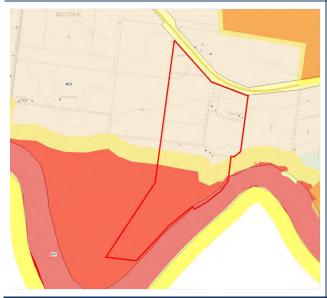
Map Applicability



Wetlands

The site is identified as being affected, in part, by Wetlands, namely the Murray River (**Appendix G**).

The land identified predominantly affects the southern-most portion of the land and the land adjacent the Murray River. A small portion of land along the southern edge of HPN 1 is located within the Wetlands overlay. Notwithstanding, the land appears to have already been compromised by historical agricultural practices occurring on the land.



Bushfire Prone Land

A portion of the site is affected by Bushfire Prone Land (**Appendix H**). The affected land largely pertains to the southernmost portion of the land which is identified as Vegetation Category 1 which typically consists of forest, woodlands, heaths (tall and short), <u>forested wetlands</u> and timber plantations.

A portion of the southern parts of HPN 1 and 2 are located within the 100m Vegetation Buffer. Notwithstanding, the affected vegetation comprises existing vineyards and established landscaping surrounding existing dwellings and ancillary buildings. No planting or removal of vegetation is proposed as part of this application.

4.2 Permit Triggers

4.2.1 Demolition

Having regard to clause 2.7 of the LEP, the proposal does not incorporate the demolition of a building or work which may be carried out only with development consent.



4.2.2 Heritage Conservation

Having regard to clause 5.10(2) of the LEP, the proposal does not incorporate activities associated with heritage conservation where development consent is required.

4.2.3 Earthworks

The proposal incorporates earthworks that are:

- Exempt development under Wentworth LEP 2011, Part 7.1, Clause 1(b) as the earthworks to be undertaken are considered minor in nature only; and
- Exempt development under Wentworth LEP 2011, Part 7.1, Clause 2(a) as the earthworks to be undertaken are exempt development under the LEP and SEPP (Exempt and Complying Development Codes); and
- Exempt development under SEPP (Exempt and Complying Development Codes), Subdivision 15,— Earthworks, retaining walls and structural support, as the works will comply with the criteria outlines in Clause 2.30.

Development consent is therefore not required for the proposed earthworks.

4.2.4 Category of Development Consent for Use

The Wentworth LEP2011 includes the subject site in the RU1 – Primary Production Zone.

The Locality and Zoning Plan in **Attachment A** depicts the zoning of the site and its neighbourhood.

The proposal falls within the definitions of a 'farm building' under the LEP, which is defined as:

"... a structure the use of which is ancillary to an agricultural use of the landholding on which it is situated and includes a hay shed, stock holding yard, machinery shed, shearing shed, silo, storage tank, outbuilding or the like, but does not include a dwelling".

The categories of development consent that are prescribed under the Land Use Table for the TU1 – Primary Production Zone for the defined uses that comprise the development are set out in **Table 9**.

Table 9: Categories of Development

Defined Use	Development Consent
Farm Building	Permitted with consent

The overall category of development consent for the application to use the site for the purposes of the proposal is determined to be permitted with consent.



5 Local Planning Assessment

5.1 Local Environmental Plan

5.1.1 Zone objectives

An assessment of the proposal against the objectives of the RU1 – Primary Production Zone is set out in **Table 10**.

Table 10: Assessment Against Zone Objectives

Objective	Assessment Comments
To encourage sustainable primary industry production by maintaining and enhancing the natural resource base.	The proposed HPN structures will not prejudice the land for primary production. The land is currently used for the growing of grapes.
To encourage diversity in primary industry enterprises and systems appropriate for the area.	The proposed HPN structures will enable continuation of the land for primary production and provide opportunities for diversification of produce.
To minimise the fragmentation and alienation of resource lands.	The proposal does not seek to change the existing use of the land or provide for opportunities to sub-divide the land.
To minimise conflict between land uses within this zone and land uses within adjoining zones.	The proposal does not seek to change the existing use of the land or provide for opportunities to sub-divide the land.
To encourage and promote the growth and diversification of economic and employment opportunities in agriculture, horticulture and tourism.	The proposed HPN structures will protect crops from unseasonable weather events and allow for the continued use of the land for horticultural purposes.
To enable the development of restaurants and cafes and kiosks as part of agritourism development.	Not applicable.

In summary, it is assessed that the proposal will not conflict with the objectives of the RU1 – Primary Production Zone.

5.1.2 Principal Development Standards

There are no principal development standards in the LEP that are relevant to the assessment of the proposed development. The LEP defers to the assessment provisions outlined in the relevant State Environmental Planning Policies.

5.1.3 Miscellaneous Provisions

There are no miscellaneous provisions that are relevant to the assessment of the proposal.



Compliance Achieved

5.1.4 Additional Local Provisions

The additional local provisions (Part 7 of the Wentworth LEP 2011) that are relevant to the assessment of the proposal are:

- Provision 7.4 Terrestrial Biodiversity
- Provision 7.5 Wetlands
- Provision 7.7 Riparian Land and Murray River and other watercourses general principles

Having regard to Provision 7.5, the assessment against the relevant additional local provisions are contained in **Table 11**.

Table 11: Wentworth LEP 2011 Additional Local Provisions

Provision

Provision 7.4 - Terrestrial Biodiversity □ Complies The objective of this clause is to maintain terrestrial For the following reasons: biodiversity by-The land is identified in the State Government's ePlanning protecting native fauna and flora, and Spatial Viewer as being affected by Terrestrial protecting the ecological processes necessary for Biodiversity. This largely applies to the land within the their continued existence, and southern portion of the site which is directly adjacent the encouraging the conservation and recovery of Murray River and which does not comprise any built form. native fauna and flora and their habitats. The proposed HPN structures will cover existing vineyards and will not adversely impact upon any land containing This clause applies to land identified as "Terrestrial native vegetation or which has not been historically Biodiversity" on the Natural Resource-Terrestrial cleared for horticultural purposes. Biodiversity Map. Before determining a development application for development on land to which this clause applies, the consent authority must consider whether or not the developmentis likely to have any adverse impact on the condition, ecological value and significance of the fauna and flora on the land, and (b) is likely to have any adverse impact on the importance of the vegetation on the land to the habitat and survival of native fauna, and has any potential to fragment, disturb or diminish the biodiversity structure, function and composition of the land, and is likely to have any adverse impact on the habitat elements providing connectivity on the land. Development consent must not be granted to development on land to which this clause applies unless the consent authority is satisfied thatthe development is designed, sited and will be managed to avoid any significant adverse environmental impact, or if that impact cannot be reasonably avoided—the development is designed, sited and will be managed to minimise that impact, or



	Provision	Compliance Achieved
(c)	if that impact cannot be minimised—the development will be managed to mitigate that impact. pendix E for map).	
	1 7.5 – Wetlands	☑ Complies
wee de de 2. Th the 3. Wh de coi im (a) (b) (c) (d) (e) 4. Be cla tha (a) (b)	the condition and significance of the native flora on the land and whether it should be substantially retained, and the provision and quality of habitats for indigenous and migratory species, and the surface and groundwater characteristics of the site, including water quality, natural water flows and salinity, and any wetland in the vicinity of the proposed development and any proposed measures to minimise or mitigate those impacts. fore granting consent to development to which this cause applies the consent authority must be satisfied at— the development is sited, designed and managed to avoid potential adverse environmental impacts, or	 The site is identified as being affected, in part, by Wetlands, namely the Murray River (Appendix G). The land identified predominantly affects the southern-most portion of the land and the land adjacent the Murray River. A small portion of land along the southern edge of HPN 1 is located within the Wetlands overlay. Notwithstanding, the land appears to have already been compromised by historical agricultural practises occurrin on the land. The proposed HPN structures (including anchors and arbours) will not be located within any designated wetland, nor will they restrict the flow of water over the land.
	n 7.7 – Riparian Land and Murray River and Other urses – General Principles	© Complies
	e objective of this clause is to protect and maintain	For the following reasons: The site is identified as being affected, in part, by Riparian
the (a) (b) (c)	water quality within the Murray River and other watercourses, the stability of the bed and banks of the Murray River and other watercourses, aquatic riparian habitats,	Lands and Watercourse, namely the Murray River located adjacent the south-eastern boundary of the site (Appendix F). The proposed HPN structures will not be located within any portion of the site affected by the watercourse and will be setback a minimum of 60 metres from the edge of
(d)	ecological processes within the Murray River and other watercourses and riparian areas.	the Murray River.
2. Th	is clause applies to land—	
(a)		

Resource-Watercourse Map, and



			Provision
	(b)	a wa	ited within 40 metres of the top of the bank of tercourse (being a watercourse situated on referred to in paragraph (a)).
3.	out o	develo	ermining a development application to carry pment on land to which this clause applies, it authority must consider whether or not the ent—
	(a)		ely to cause any adverse impact on the wing—
		(i) (ii)	the water quality and flows within a watercourse, aquatic and riparian species, habitats and ecosystems,
		(iii)	the stability of the bed, shore and banks of a watercourse,
		(iv) (v)	the free passage of fish and other aquatic organisms within or along a watercourse, any future rehabilitation of a watercourse and riparian areas, and
	(b)	will i	ncrease water extraction from a watercourse.
4.	deve	elopme	ent consent must not be granted to ent on land to which this clause applies unless at authority is satisfied that—
	(a)	man	development is designed, sited and will be aged to avoid any significant adverse ronmental impact, or
	(b)	if tha feasi desig	at impact cannot be avoided by adopting ible alternatives—the development is gned, sited and will be managed to minimise
	(c)	if tha	impact, or at impact cannot be minimised—the elopment will be managed to mitigate that act.
(*see	е Арре	endix F	for map).

5.2 Development Control Plan

The relevant Wentworth Shire Development Control Plan 2011 (DCP) supplements the provisions of the LEP The purpose of the DCP is provide quality development and sustainable environmental outcomes.

The DCP must be read in conjunction with the LEP; and any relevant State Environmental Planning Policies (SEPPs). Where there is a conflict between a provision in the DCP and a provision in an Environmental Planning Instrument (EPI), for example a State Environmental Planning Policy or Local Environmental Plan, the provisions of the EPI shall prevail to the extent of that inconsistency.

There are no relevant chapters of the DCP in this instance, particularly given that the use of the land is established and the proposed structures will retain a level of transparency so as not to adversely affect the rural amenity.



6 State Planning Assessment

6.1 State Environmental Planning Policies

State Environmental Planning Policies (SEPPs) specify planning controls for certain area and/or types of development and are prepared under Part 3 of the EP&A Act. SEPPs prevail over the provisions contained within a Local Environment Plan and the Development Control Plan. Clause 1.9 within the Wentworth LEP 2011 states:

This Plan is subject to the provisions of any State environmental planning policy that prevails over this Plan as provided by section 3.28 of the Act.

6.1.1 Relevant SEPP

The proposal is regulated by the following State Environmental Planning Policies (SEPP):

- SEPP (Biodiversity and Conservation) 2021: Excluded (pub. 21-10-2022)
- SEPP (Biodiversity and Conservation) 2021: Land Application (pub. 02-12-2021)
- SEPP (Exempt and Complying Development Codes) 2008: Land Application (pub. 12-12-2008)
- SEPP (Housing) 2021: Land Application (pub. 26-12-2021)
- SEPP (Industry and Employment) 2021: Land Application (pub. 02-12-2021)
- SEPP (Planning Systems) 2021: Land Application (pub. 02-12-2021)
- SEPP (Primary Production) 2021: Land Application (pub. 02-12-2021)
- SEPP (Resilience and Hazards) 2021: Land Application (pub. 02-12-2021)
- SEPP (Resources and Energy) 2021: Land Application (pub. 02-12-2021)
- SEPP (Sustainable Buildings) 2022: Land Application (pub. 29-08-2022)
- SEPP (Transport and Infrastructure) 2021: Land Application (pub. 02-12-2021)

6.1.2 Assessment against relevant SEPP

A comprehensive assessment of the proposed development against the relevant the SEPP's is provided in **Appendix K** of this report. The assessment demonstrates that the proposed development will achieve the objectives identified in the SEPPs.



7 Assessment Against Other Matters

7.1 Planning Agreements

There are no planning agreements that apply to the site.

7.2 Impacts of the Development

An assessment against the likely impacts of the development, including environmental impacts on both the natural and built environments, and social and economic impacts in the locality follows.

7.2.1 Impacts on Traffic and Access

The proposed development is anticipated to generate minimal traffic movements associated with:

- Construction materials being delivered to the site.
- Installation specialists being on-site during construction.

The number and frequency of truck movements will be minimal and largely contained within the site boundaries. It is not anticipated that any loading/unloading or works within the shoulder of the adjacent Sturt Highway will be required. Should the need arise for these works to occur the direction of vehicle and truck movement on the adjacent local road network will be in an east/west direction travelling to/from Mildura and the subject land.

7.2.2 Impacts on Site Infrastructure

There are easements and rights of carriage over the subject land for the purposes of pipelines, a pump station and vehicle access. The proposed HPN structures will not restrict access to these site facilities.

Dial before you Dig records of services infrastructure of the site indicates that the site is connected to electrical and telecommunications infrastructure.

Overhead powerlines are located within proximity of the dwellings located on-site, along the verge directly adjacent Sturt Highway and adjoining the right of carriageway which provides vehicle access to the site. We note that there are no high-tension poles located on the subject land. The proposed HPN structures will be offset a suitable distance from the electrical poles (i.e., at least 4 metres) and will not exceed 5 metres in height which is below that of the electrical cables. The proposed HPN structures will not restrict access to electricity infrastructure.



A detailed investigation is required to ensure the location of all electrical equipment prior to any excavation or other construction. Development application conditions will be met, and necessary further investigations undertaken prior to any development.

The site does not have access to reticulated urban sewer or water mains. There is an easement over the land which provides for water to be pumped from the adjacent Murray River to the site.

An Infrastructure Agreement is not applicable to the site.

Easements and Rights of Carriage are detailed on the Certificate of Title contained in **Appendix C**, whilst Dial Before You Dig mapping is contained in **Appendix D**.

7.2.3 Impacts on Visual Amenity

The proposed development will be visible from the adjacent sites and from Sturt Highway within proximity of the site boundaries.

Impacts on residential dwellings within proximity of the site will largely be minimised by generous separation distances. Dwellings on the northern side of Sturt Highway will have views of HPN 3, however impacts will be minimised due existing vegetation along the road boundaries and the separation distance, which will be no less than 190 metres. In addition, the topography of the subject land is such that it gently falls away from the road towards the Murray River, as such the land sits at a lower level than the northern properties which will reduce impacts of height.

Proposed HPN 3 will largely obscure views of HPN 2. Proposed HPN 1 will be setback further from Sturt Highway (approximately 335m from the Sturt Highway site boundary). Again, views will be partially obscured by distance and existing vegetation including vineyards located on the western adjoining property. The dwellings located to the east and west of the subject land are ancillary to primary production activities, with vineyards being the dominant land use on both sites. Residential amenity is somewhat lower than what is expected in residential zones as the associated agricultural activities are the primary focus of the land. As such, farm buildings are an anticipated form of development.

Whilst the proposed structures will be visible from the adjacent land, the structural form, materials and external appearance are not outside of the parameters of the type of development anticipated in the RU1 zone or agricultural land. The materials and colours proposed will prevent undue reflection/glare and will retain a level of transparency that enables views to adjoining land. In addition, the structures will be sited as far as possible from boundaries and adjacent residential development.

7.2.4 Impacts on Terrestrial Biodiversity

The site is identified as containing Terrestrial Biodiversity as indicated on the maps provided in the State Government's ePlanning Spatial Viewer (refer **Appendix E**).



The portion of the site affected by terrestrial biodiversity is contained within the southern-most portion of the land which lies adjacent to the Murray River. Proposed HPN 2 will be located approximately 40 metres from the affected land whilst HPN 1 will directly adjoin the affected land. Notwithstanding, impacts are minimised by the fact that the land has already been compromised by historical agricultural practises occurring on the land. HPN 1 will cover an existing vineyard and will not require the removal or disturbance of native vegetation, and excavation will be limited to a depth of 600 millimetres below natural ground level to secure the intermittent posts. HPN 2 will also be built over an existing vineyard and is separated from the terrestrial biodiversity land by an existing dwelling, farm buildings and a right of carriageway.

The proposed development seeks to allow for ongoing agricultural practises on the land with the proposed HPN providing protection to crops/orchards from unseasonable weather events. The development will not materially impact on sensitive biodiverse land as the structures extend over land which has historically been cleared for horticultural purposes and does not require the clearance of native vegetation.

7.2.5 Bushfire Risks

The site is identified as Bushfire Prone Land – Vegetation Category 1 and Vegetation Buffer.

Notwithstanding, the affected land largely pertains to the southern-most portion of the land which is devoid of built form and comprises vegetation and wetlands.

The proposed structures are not encouraging habitation through the creation of additional dwellings or a land use aimed at providing occupation for vulnerable persons.

The proposed HPN structures will cover existing farmland, will not restrict evacuation, and will not restrict access for fire fighting vehicles in the event of a bushfire emergency.

The subject site is relatively developed, having been used for agricultural purposes for a number of years. With the exception of the southern-most portion of the site, it is largely devoid of vegetation. Some vegetation is evident along road verges, internal road tracks and surrounding existing dwellings on-site. The proposed development does not involve the planting or removal of vegetation, nor does it restrict any existing internal tracks or vehicle access points.

7.2.6 Impacts on Riparian Lands and Watercourses

The site is identified as being affected by Riparian Land and Watercourses, namely the Murray River located adjacent the south-eastern boundary of the site (**Appendix F**).

The proposed HPN structures will be located at least 60 metres from the affected portion of land, will only occur over land that has been historically cleared for horticultural purposes, and will not restrict the flow of water over the land. No portion of the proposed structures including the anchors or arbours will be located within the watercourse.



7.3 Suitability of the Site

The site is assessed to be suitable for the development for the following reasons:

- The site is used for existing agricultural purposes and has been used for this purpose for decades.
- The site is located within RU1 Primary Production Zone, where farm buildings are permitted with consent.
- Construction works will predominantly occur on-site with minimal vehicle movements through the existing crossover or to the adjacent road network.
- Visual and environmental impacts are suitably avoided and mitigated where necessary, with sufficient setbacks from sensitive land uses (residential dwellings).



8 Conclusion

This SEE has been prepared by MasterPlan in support of an application made by G2 Netting Group seeking a development consent for a proposal to install three (3) hail proof netting (HPN) structures. The application is made to the Council under the EP&A Act.

The Development Application is made over land located at 5721B and 5758 Sturt Highway, Monak (the 'subject land' or 'site').

This report has demonstrated that the proposal is a suitable development for the site. The assessments contained in this report conclude that:

- The site is suitable for the intended purpose of the proposal.
- The intended development of the site is compatible with the locality.
- The nature and scale of the proposal is suitable for the local context.
- The proposal will not introduce adverse impacts on the environment that are not able to be mitigated.

In addition, our assessment has determined that:

The proposal responds well to the zoning and surrounding character of its locality and achieves a scale and form of development that is consistent with community expectations as expressed through local and State planning instruments.

- The proposal is consistent with the objectives of the LEP.
- Complies with the relevant provisions of the DCP.
- Will achieve the objectives of the relevant SEPP.
- Will not result in significant adverse impacts on the environment.

Our assessment in consideration of the requirements of all relevant statutory planning instruments under the EP&A Act is that there are strong grounds for Council to approve the development application subject to reasonable and relevant conditions.

Jasmine Walters

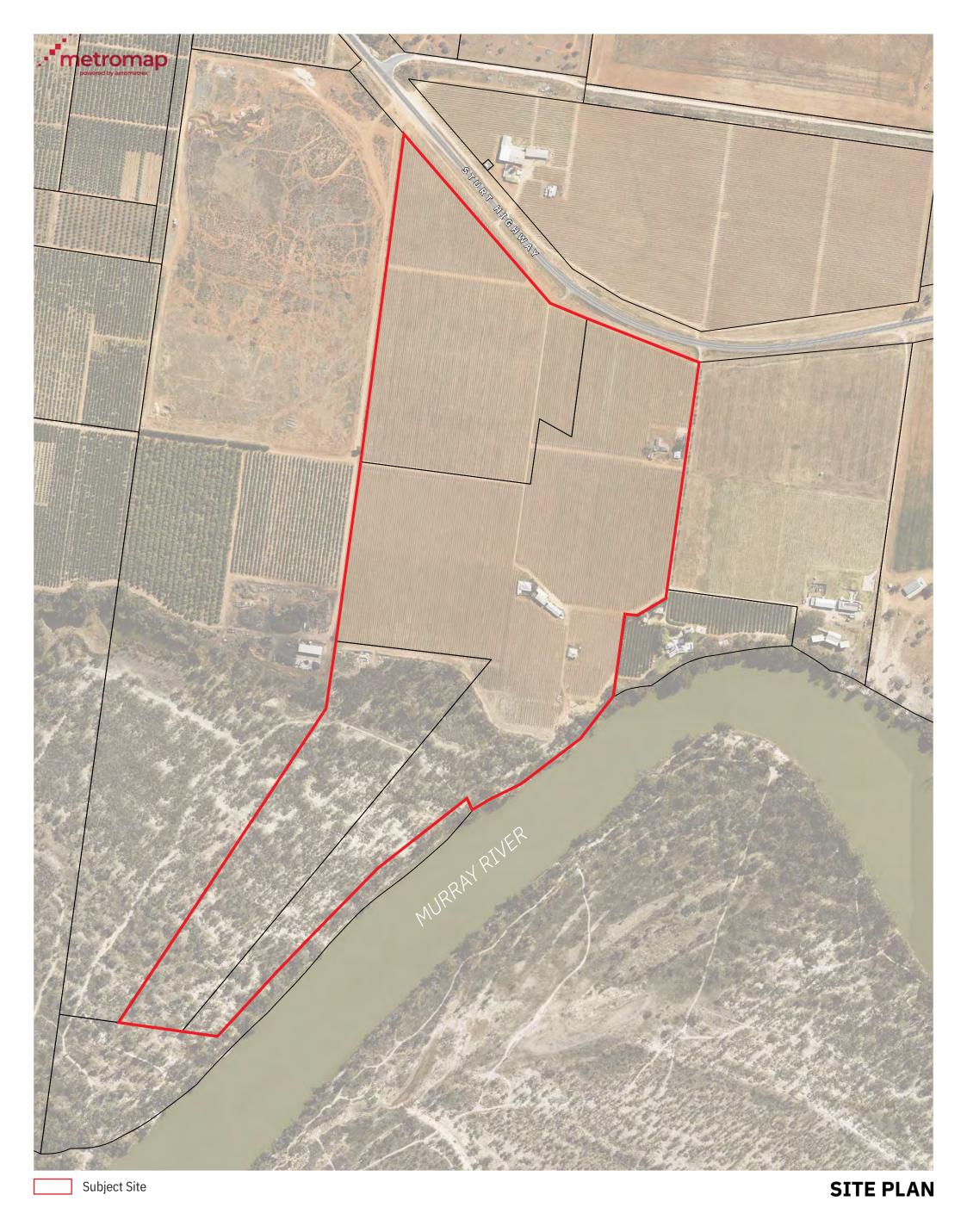
MPIA

Bachelor of Urban and Regional Planning (Hons.)



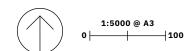
Appendix ASite, Locality and Zone Plan



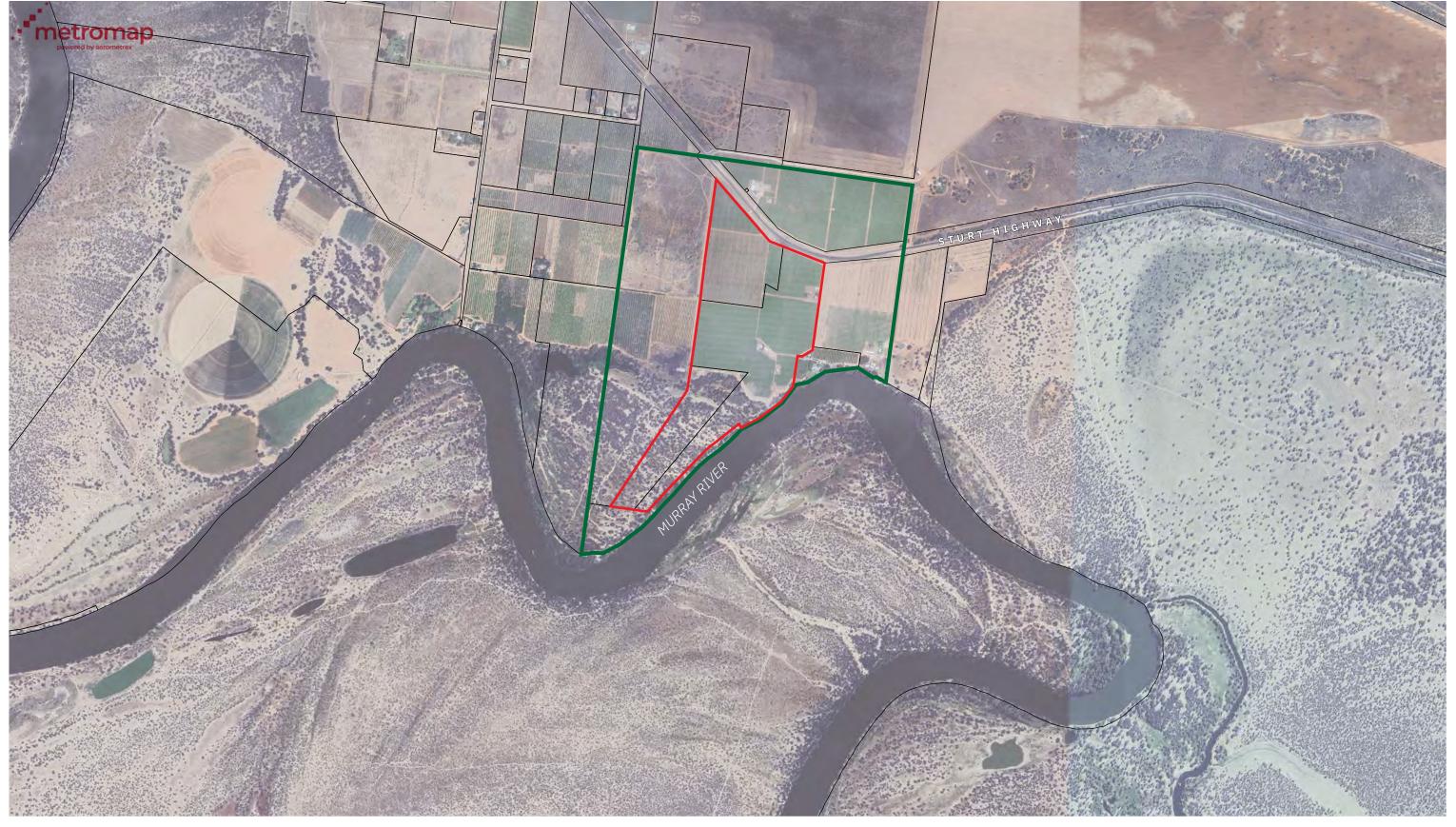


5721B Sturt Highway MONAK

for Marciano Table Grapes



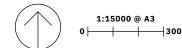




Subject Site Locality **LOCALITY PLAN**

5721B Sturt Highway MONAK

for Marciano Table Grapes







Subject Site

SP2

RU1 Primary Production

State Highway

ZONE PLAN

5721B Sturt Highway MONAK

for Marciano Table Grapes





Appendix BProposed Plan





DA - Existing Site Plan

1:3000

1:3000 Scale Bar

STRUCTURE LEGEND STRUCTURE HEIGHT: 5.0 METRES SITE BOUNDARY EASEMENTS POWER LINE CLEARANCE

No.	Revision Information	Ву	Date
			-

Structure Height

Flat Top Structure Height (H)



THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Project Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

Drawing Title **EXISTING SITE PLAN**

Client Name:

P&T Marciano Scale @ A1 As indicated Checked

HH JG2
Project No. Sheet No. Rev.

1759 - 101 - .



STRUCTURE LEGEND

STRUCTURE HEIGHT:

5.0 METRES

TOP NETTING TYPE:

Construction: Lock stitch knitted HDPE monofilament

20mm Hexagonal hole with cross over

Weight of Net: 75 grams/mtr

Nominal shade factor: 12%



SITE BOUNDARY

EASEMENTS

POWER LINE CLEARANCE

PROPOSED NETTING STRUCTURE

ANCHOR LINE

THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Project Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

No. Revision Information

Flat Top Structure Height (H)

Structure Height

Drawing Title PROPOSED SITE PLAN

Client Name:

P&T Marciano Scale @ A1 As indicated

Checked

HH JG2
Project No. Sheet No. Rev.

1759 - 102 - .

214.4 m 239.6 m

Site - Plan (Sales)

1:1000

Drawing Approvals

These drawings have been reviewed by the client and approved for installation. Any variation, alteration, change or modification to the design and/or materials, following this approval, must be in writing and signed by the client or their authorised representative, and the company reserves the right to vary the quotation accordingly.

Date:

FOR APPROVAL Sheet List - Sales Drawing Sheet Name 1759-001 SITE PLAN 1759-002 DETAIL SHEET 01

Structure Height

Flat Top Structure Height (H)

Ref G2 Code Description

1616 QNW161630 16mm 16x300m White Quad Crossover

Wire and Cable

Double Cable / Wire
7.5mm Cable 6mm Cable 3.15mm Wire High Tensile 3.15mm Spring Wire 2.65mm Wire High Tensile

Line Types

Site Boundary = — — Easement Locations

──V──V Overhead Powerlines - Low Voltage —√—√— Overhead Powerlines - High Voltage Fence Line



THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT AUTHORITIES, APPLICABLE AUSTRALIAN STANDARDS AND THE BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS ON SITE BEFORE COMMENCING ANY WORK OR MAKING SHOP DRAWINGS. FIGURED DIMENSIONS ARE NOT TO BE USED, SCALED DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

Drawing Title

SITE PLAN

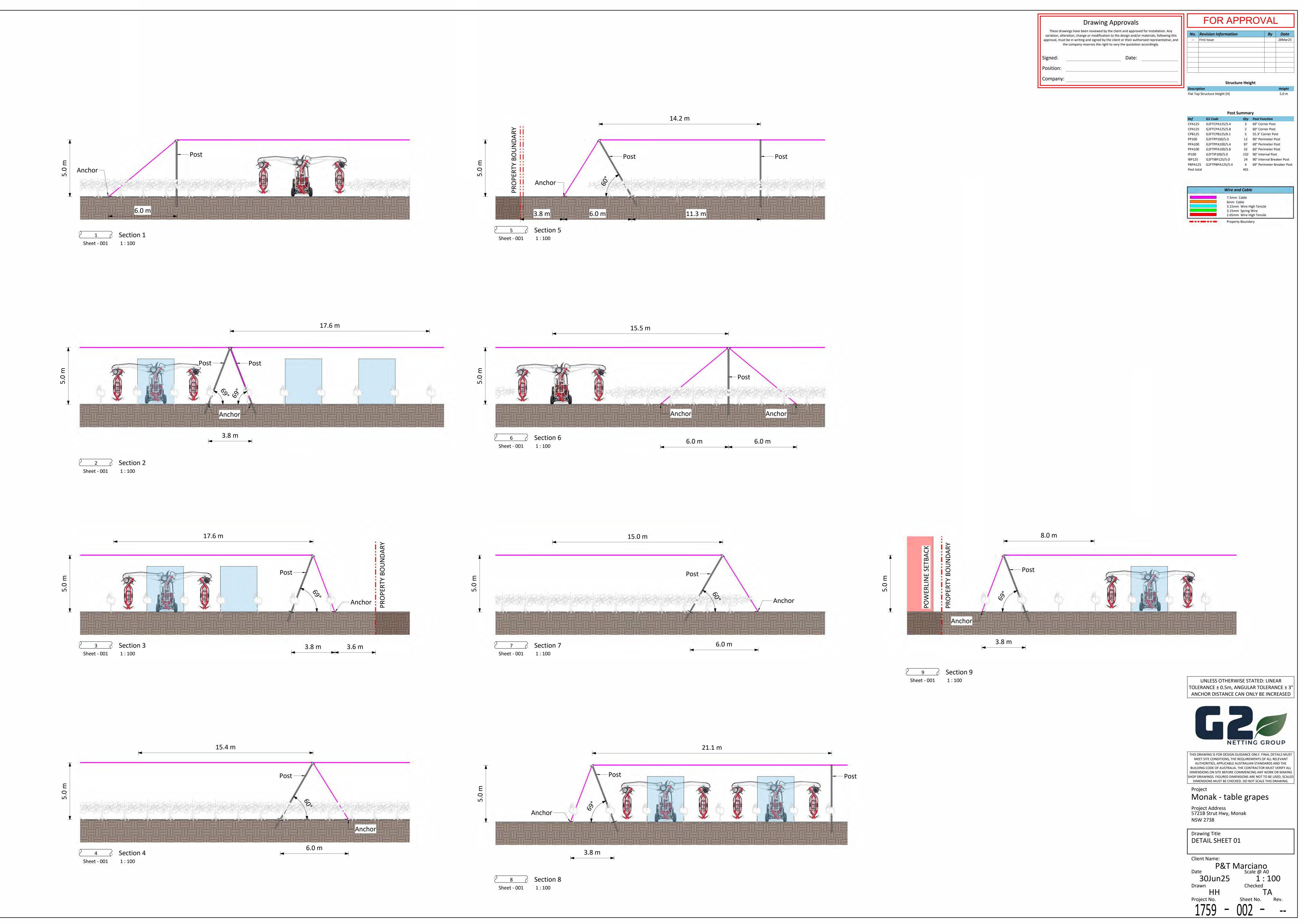
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Project No.

Client Name: P&T Marciano

Checked

Sheet No. 1759 -



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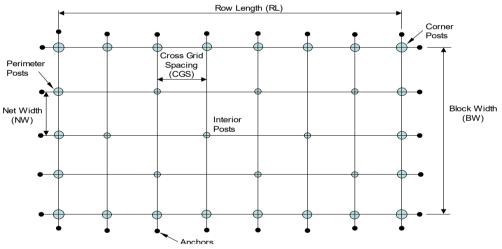
FLAT TOP Structure Evaluation Spreadsheet V2024-09

This spreadsheet is used to provide design guidance for a flat top structure.

Quote, Client & Block ID: 1759-CR01_P&T_Marciano_StructType_27May25

Basic Layout

,			
Description	Variable	Value	Units
Factor of Safety (Failure)	FoS	1.25	
Regional Wind Speed (V ₁₀₀ , Region A0 , AS/NZS 1170.2:2021)	V_R	41.0	m/s
Climate Change Multiplier (Table 3.3)	M_C	1.0	
Wind Direction Multiplier (Table 3.2A)	M_{D}	1.0	
Terrain/Height Multiplier (Table 4.1(A) Terrain Category 2)	$M_{Z,cat}$	0.91	
Shielding Multiplier (Section 4.3)	M_S	1.0	No shielding
Topographic Multiplier (Section 4.4)	M_{T}	1.0	Mh = 1.0, slope < 0.05
Site Wind Speed (Section 2.2)	$V_{sit,B}$	37.3	m/s
Design Wind Speed (for a structure height of 5.0m)	V_{MW}	37.3	m/s
besign with speed (for a structure fielght of s.om)	• MW	135	km/hr
Design Distributed Hail Loading	W_hail	3.0	kg/m ²
			I
Structure Height	Н	5.0	m
Average Net Width	NW	19.4	m
Number of Net Runs	nNR	13.0	# rows
Cross-Grid Spacing	CGS	15.5	m
Block Length	RL	288.0	m
Block Width	BW	251.0	m
Interior Post Configuration	Sta	ggered	



Anchors								
Zone	1	2	3	Max Area				
Structure Height	5.0	5.0	5.0	5.0				
Max Net Width	19.4	20.8	20.8	19.4				
Number of Net Runs	13	13	13	13				
Cross-Grid Spacing	15.5	15.5	15.5	15.5				
Block Length	288	216.5	229.8	288				
Block Width	251	235	235	251				
Hail Load per Bay (kg):	902	967	967	902				
Area Row Direction	5587	4503	4780	5587				
Area CG Direction	3891	3643	3643	3891				

SUMMARY of the Margins of Safety

Cable - 1x7 Galv 7.5 mm 1770	MS_{MIN}	0.01	See Cables worksheet
Corner Post (B2 SE) - 90deg Config - 125NB Medium / Grade 250	MS_{MIN}	0.14	See CP_90 worksheet
Corner Post (B2 SE) - Insert - 100NB Heavy / Grade 300	MS _{MIN}	0.53	See CP_90 worksheet
Corner Post (B2 SE) - Footings - Cast-In-Place Concrete	RtoR	1.32	See CP_90 worksheet



Corner Post (TP) - 69deg Config - 125NB Medium / Grade 250	MS_{MIN}	0.15	See CP_69 worksheet
Corner Post (TP) - Insert - 100NB Heavy / Grade 300	MS _{MIN}	0.61	See CP_69 worksheet
Corner Post (TP) - Footings - Cast-In-Place Concrete	RtoR	1.22	See CP_69 worksheet
Corner Post (Angled) - 60deg Config - 125NB Medium / Grade 250	MS _{MIN}	0.30	See CP_60 worksheet
Corner Post (Angled) - Insert - 100NB Heavy / Grade 300	MS_{MIN}	0.83	See CP_60 worksheet
Corner Post (Angled) - Footings - Cast-In-Place Concrete	RtoR	1.36	See CP_60 worksheet
Corner Post (55deg) - 55deg Config - 125NB Medium / Grade 250	MS _{MIN}	0.10	See CP_55 worksheet
Corner Post (55deg) - Insert - 100NB Heavy / Grade 300	MS_{MIN}	0.71	See CP_55 worksheet
Corner Post (55deg) - Footings - Cast-In-Place Concrete	RtoR	1.08	See CP_55 worksheet
Perimeter Breaker Post (SE) - 69deg Config - 125NB Medium / Grade 350	MS_{MIN}	0.31	See PBP_69_SE worksheet
Perimeter Breaker Post (SE) - Insert - 100NB Heavy / Grade 300	MS_{MIN}	0.46	See PBP_69_SE worksheet
Perimeter Breaker Post (SE) - Footings - Cast-In-Place Concrete	RtoR	1.01	See PBP_69_SE worksheet
Perimeter Breaker Post - 69deg Config - 125NB Medium / Grade 250	MS _{MIN}	0.08	See PBP_69 worksheet
Perimeter Breaker Post - Insert - 100NB Heavy / Grade 300	MS _{MIN}	0.53	See PBP_69 worksheet
Perimeter Breaker Post - Footings - Cast-In-Place Concrete	RtoR	1.10	See PBP_69 worksheet
Interior Breaker Post - 125NB Medium / Grade 250	MS_{MIN}	0.37	See IBP worksheet
Interior Breaker Post - Insert - 100NB Heavy / Grade 300	MS _{MIN}	0.74	See IBP worksheet
Interior Breaker Post - Footings - Rammed Insert	RtoR	1.07	See IBP worksheet
Perimeter Post (TP) - 69deg Config - 100NB Light / Grade 350	MS_{MIN}	0.26	See PP_TP worksheet
Perimeter Post (TP) - Insert - 90NB Heavy / Grade 300	MS_{MIN}	1.27	See PP_TP worksheet
Perimeter Post (TP) - Rammed Insert	RtoR	1.07	See PP_TP worksheet
Perimeter Post (CG 69deg) - 69deg Config - 100NB Light / Grade 350	MS _{MIN}	0.20	See PP_69 worksheet
Perimeter Post (CG 69deg) - Insert - 90NB Heavy / Grade 300	MS_{MIN}	1.19	See PP_69 worksheet
Perimeter Post (CG 69deg) - Rammed Insert	RtoR	1.00	See PP_69 worksheet
Perimeter Post (RE) - 60deg Config - 100NB Light / Grade 350	MS _{MIN}	0.13	See PP_60 worksheet
Perimeter Post (RE) - Insert - 90NB Heavy / Grade 300	MS_{MIN}	1.29	See PP_60 worksheet
Perimeter Post (RE) - Footings - Rammed Insert	RtoR	1.00	See PP_60 worksheet
Interior Post - 100NB Light / Grade 350	MS _{MIN}	0.61	See Interior_Post worksheet
Interior Post - Footings - Rammed Insert	RtoR	1.20	See Interior_Post worksheet
Post Guys - One loop of 1x7 Galv 7.5 mm 1770	MS_{MIN}	0.26	See Guys worksheet
Anchors - AU350 Jumbo Type Drill Anchor	MS_{MIN}	0.28	See Anchors worksheet

MS = Margin of Safety = Allowable Load / (FoS x Applied Load) - 1 where FoS = Factor of Safety RtoR = Ratio to Requirement = Allowable Load / Applied Load

Critical Modes of Failure - Calculated using "Margin of Safety" criteria.

- 1. Cable break One cable breaking would result in a load redistribution and likely higher loads on neighbouring cables.
- 2. Anchor Failure One anchor failing would result in a load redistribution and likely higher loads on neighbouring anchors.

Non-Critical Modes of Failure - Calculated using "Margin of Safety" criteria.

- 1. Corner or perimeter post buckling and/or bending failure Results in a loss of tension, but it will remain able to take load as long as no critical modes occur.
- 2. Interior post buckling and/or bending failure This will bend until the load goes elsewhere. For example the hail would hit the ground itself and therefore reduce the loading on the interior post. The structure will remain intact as long as no critical failures occur.

Safe but Undesirable Modes of Failure - Calculated using the "Ratio to Requirement" criteria.

1. Exceeding footing or pile allowable loads will result in a slackening of cable tension, with no immediate structural implications.

Certification Statement

I verify that the above structure has been evaluated, using classical engineering methods and tools, and found to have acceptable margin of safety against both the specified wind and hail load conditions.

BY: Robert Grigson BE (Mech), ME (Aero) DATE: 27Mar25



Loadings

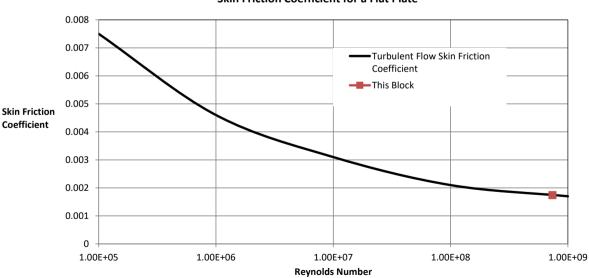
1759-CR01_P&T_Marciano_StructType_27May25

The following inputs are used to size the structure. The most significant is the net drag coefficient and lateral deflections at the top of the perimeter and corner posts due to cable straining.

			_
-	-		ts
•	u	U	LS

Description	Variable	Value	Units	Comments
Cable pre-tension during installation	P_{T0}	1500	kg	This is the maximum tension each cable is pulled during straining and subsequent net installation.
Block Reynolds Number	Re	7.4E+08	ı	Velocity x Length / Kinematic Viscosity
Flat Plate Skin Friction Coefficient	Cf	0.0017		Based on Stanford University data. Assumes turbulent flow, and the Reynolds number above.
Net Drag Coefficient (Roof)	Cdw	0.01		A value of 0.01 is used. This is selected to be greater than the skin friction coefficient to cover profile and interference drag, and remain conservative. A lower number may be used later as long as it is supported by test data.
Distributed Aero Loading on Roof	W_aero	0.88	kg/m ²	Aero loading on net per meter squared
Wall Net Optical Porosity	β	8mm Quad Net 74%		Optical porosity = 0 for no porosity. Can be computed as the area of holes divided by the total area. Aerodynamic porosity and Drag coefficient from "A wind tunnel study of windbreak
Wall Net Aerodynamic Porosity	α	89%		drag", by Guan, Zhang and Zhu (China). 8mm Quad Net = 74%, 50% Shade Cloth = 50%, Canopy Net = 86%.
Wall Net Drag Coefficient	Cdw	0.21		Computed from optical porosity. Note drag CG assumed to be acting at 11/18 of the structure height.
Distributed Wall Net Loading	Ww_aero	18.5	kg/m ²	Aero loading on net per meter squared of wall net.
Distributed Hail Loading	W_hail	3.0	kg/m ²	The maximum hail load per square meter must be greater than
Total Hail Load per Bay	W	902	kg	2.0 at all times for Flat Top Structures. Clients may wish to have more capability therefore this should be set between 2.0 and 5.0.
Maximum Corner and Perimeter Post Top Deflection after Cable Straining	δу_рр	50	mm	Use 1/2 diameter of the post, applicable to corners and perimeters. After straining the cables during installation, the post setting must not be greater than 1/2 diameter over the length.
Interior Post Lateral Deflection	δy_ip	83	mm	Applicable to Interior Post bending analysis. A post is very strong in compression, however this reduces significantly under the onset of bending loads. This criteria condition assumes there is significant wind forcing the top of the post lateral and inducing significant bending.
Maximum Net Tension Capability	Pnet	100	kg/m	Determined from test, not used on this analysis.
Maximum Wall Net Tension	Pwall_net	50	kg/m	Determined from test for correctly set wall nets (assumes 8mm quad wall net).

Skin Friction Coefficient for a Flat Plate



Cables

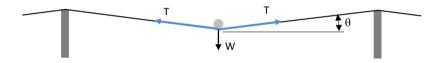
1759-CR01_P&T_Marciano_StructType_27May25

Comments

The cables must be able to support the load due to maximum wind, load due to maximum hail, and a hybrid case of 75% wind speed combined with maximum hail. The maximum wind load is obtained for a cable by totalising the total net shear drag load along the full length of the cable. This is conservative due to the fact that the attached lateral cables and interior posts take a small portion of the load (the interior posts bend back with cable stretch, and the lateral cables form a point loaded catenary). The maximum hail load arises from a cable taking the maximum hail load as a point load in between vertical supports. Two further hybrid cases combine the cable load from a 75% wind speed with cable load from maximum hail. All cable loads must be less than the cable allowable load assuming the specified factor of safety.

Variable

-1				7
Select Cable Type	1x7 (Salv 7.5 mm 1	770	
Breaking Tension		6200	kg	
Wire diameter		7.5	mm	•
Elastic Modulus		80000	N/mm ²	
Cable pre-tension during installation	P_{TO}	1500	kg	This is the peak value used during the installation.
Maximum Hail Load	W_{cable}	902	kg	Total hail loading per each Cross-Grid & Row Cable betwee supports.
Maximum Cable Load due Wind				
Wind in Row Length Direction	Area	5587.2	m^2	Wind direction parallel to Row Cables
Maximum Cable Load on Row Cable	$T_{cable_Row_Wind}$	4907	kg	
Wind in Block Width Direction	CGS*BW	3891	m^2	Wind direction parallel to Cross-Grid Cables
Maximum Cable Load on Cross-Grid Cable	$T_{cable_CG_Wind}$	3417	kg	



Maximum	Cable Lo	licH aub he	(No Pro	Tension)
IVIAXIIIIUIII	Cable Lo	au uue naii	i iivo Pre-	- rensioni

Description

Cable tension prior to Hail Loading	P_{T0}	0	kg	Assuming no cable pre-tension.
Estimated Top Cable Angle due Hail Load	θ_{Cable0}	7.8	deg	Cable angle to horizontal at support.
Top Cable Load (tensioned)	T_{cable0}	3337	kg	Cable load due to maximum hail with no initial pre-tension.
Hail load error check		0	kg	Must be zero.
Maximum Cable Load due Hail (Pre-Tensioned)				
Cable Tension due to pre-tension	P ₋₁	1500	kg	Usina the nominal cable pre-tension.

Cable Tension due to pre-tension	P_{T1}	1500	kg	Using the nominal cable pre-tension.
Estimated Top Cable Angle due Hail Load	θ_{Cable1}	6.6	deg	Cable angle to horizontal at support.
Top Cable Load (tensioned)	T_{cable1}	3915	kg	Cable load due to maximum hail with initial pre-tension.
Hail load error check		0	kg	Must be zero.

Maximum Cable Load on Row Cable (75% Wind Speed combined with maximum hail)

······································						
Effective Cable Tension due 75% Wind Load	P _{T2}	2760	kg	Using cable load due to 75% wind speed in row direction as the pre-tension		
Estimated Top Cable Angle due Hail Load	θ_{Cable2}	5.7	deg	Cable angle to horizontal at support.		
Top Cable Load (Hybrid Case Row)	T_{cable2_Row}	4547	kg	Cable load with cable pre-tensioned with wind loading.		
Hail load error check		0	kg	Must be zero.		

Maximum Cable Load on Cross Grid Cable (75% Wind Speed combined with maximum hail)

Effective Cable Tension due 75% Wind Load	P _{T3}	1922	kg	Using cable load due to 75% wind speed in cross-grid direction as the pre-tension
Estimated Top Cable Angle due Hail Load	θ_{Cable3}	6.3	deg	Cable angle to horizontal at support.
Top Cable Load (Hybrid Case Cross-Grid)	T_{cable3_CG}	4111	kg	Cable load with cable pre-tensioned with wind loading.
Hail load error check		0	kg	Must be zero.

Cable Force Adjustment Factors for the Stagge	This analysis worksheet analyses the cables based on a			
	Row_Factor	100%		staggered interior post configuration. Analytical modelling was
	CG_Factor	100%		used to compare the different interior post configurations, and these factors adjust this analysis to better represent the selected configuration. They only apply to hail only and combined hail and wind load cases.
Cable Tension Analysis				ana wina ioaa cases.
Maximum Cable Loading (Row Cables)	$T_{cable_Max_Row}$	4907	kg	The maximum of 2.0 x pre-tension, theoretical wind loading
Maximum Cable Loading (CG Cables)	$T_{cable_Max_CG}$	4111	kg	along row length, wind loading across the block, maximum hail loading and 75% wind sped combined with maximum hail from
Maximum Cable Loading (All)	T_{cable_Max}	4907	kg	the two wind directions.
Breaking Tension		6200	kg	Obtained from cable selection at top.
Margin of Safety (Cable Tensile)	MS	0.01		Must be greater than zero, includes the factor of safety

Corner Post (B2 SE)

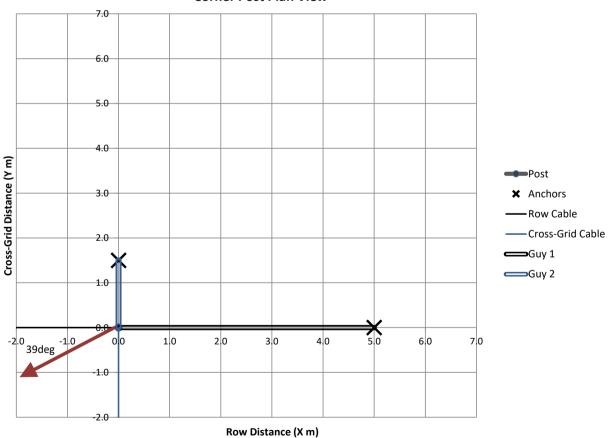
1759-CR01_P&T_Marciano_StructType_27May25

Corner posts are sized using the maximum wind loadings (roof and wall net loadings). Hail loading is considered minimal on a corner post. The analysis below assesses the anchor loadings based on no moment at the base of the corner post. In reality, a moment will exist but this will not have a significant impact on guy and cable forces. However it will have a significant impact on the post stress, and therefore is included in the stress calculations below.

Inputs

Description	Variable	Value	Units	Comments
	-			
Select Main Post Material	125NB N	/ledium / Gra	ade 250	D _{WB_Top_Row} T _{Cable May CG}
Outside Diameter	D	139.7	mm	Cable_Max_CG
Wall Thickness	t	5.0	mm	
Cross Sectional Area	Α	2116	mm^2	D _{WB_Top_CG} T _{G1} T _{Cable_Max_Row}
2nd Moment of Area	1	4805412	mm^4	
Elastic Modulus	Е	207000	N/mm ²	$/T_{G2}$
Yield Strength	Fy	250	N/mm ²	// 62 \\
Tensile Strength	Ft	320	N/mm ²	\wedge
Buckling Strength	Fc	200	N/mm ²	$A_1 \bullet \downarrow^{\theta_{G1}} \theta_{P1} $
Select Insert Material	100NB	Heavy / Grad	de 300	L ₁
Outside Diameter	D	114.3	mm	θ_{P2}
Wall Thickness	t	5.4	mm	θ_{G2}
2nd Moment of Area	1	2745389	mm^4	L ₂
Yield Strength	Fy	300	N/mm ²	A ₂
Tensile Strength	Ft	400	N/mm ²	-

Corner Post Plan View



Corner Post Configuration

Anchor Locations	A1	5.00	0.00	(m, m) assuming post base at (0,0)
	A2	0.00	1.50	(m, m) assuming post base at (0,0)
Post Angle (Viewed from CG Direction [Y])	θ_{P1}	90	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle (Viewed from Row Direction [X])	θ_{P2}	90	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle	θ_{PMIN}	90	deg	This is the minimum angle the post makes with the ground _plane
Vector on ground this is measured on		0.0	0.0	(m,m) assuming post base at (0,0)
Post Length	Lp	5.0	m	Post length above ground - these posts use an insert
Walls along row ends of block.		No Wall		Only applicable if walls are present
Walls along sides of block.		No \	Wall	Only applicable if walls are present

Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

Determination of duy Loads and Post Compres	sicii Ecaus (usi	ing Growar v	soor amate	<u> </u>
Maximum Cross-Grid Cable Load (Loading)	$T_{Cable_Max_CG}$	4111	kg	Only 1 CG Cable runs to this corner post
Maximum Row-Cable Load	T _{Cable_Max_Row}	3195	kg	TCable_Max_CG * cos 39°
Maximum Cross-Grid Cable Load	$T_{Cable_Max_CG}$	2587	kg	TCable_Max_CG * sin 39°
Percentage of perimeter cable load (Row)		70%		This compensates for the fact that only 70% of the CG
Percentage of perimeter cable load (CG)		70%		cable is netted.
Wall Net Loading applied to Top of CP (X Dir)		0	kg	
Wall Net Loading applied to Top of CP (Y Dir)		0	kg	
Wall Tension Loading applied to CP (X Dir)		0	kg	
Wall Tension Loading applied to CP (Y Dir)		0	kg	
Corner Post Load (Row)	T_{CP_Row}	2237	kg	
Corner Post Load (CG)	T_{CP_CG}	1811	kg	

The above forces act at the top of the post. The post remains in static equilibrium, and therefore the guy forces can be computed from the sum of the forces in 3 dimensions.

Guy 1 Load	T_{G1}	3163	kg	
Guy 2 Load	T_{G2}	6303	kg	
Maximum Guy Load	T_{G_Max}	6303	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	8274	kg	The maximum load at any part of the column
Post Length	Lp	5.0	m	Post length above ground - these posts use an insert
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δу_рр	50	mm	Must get the final position of the post top within this
Equivalent lateral load due this deflection	Ру	1194	N	
Bending moment due this lateral load	M1	5968322	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	4056750	Nmm	Maximum at bottom of post, assuming a square root distribution.
Combined wall net loadings	М3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height.
Stress Calculations				
Axial Stress	fa	38	N/mm ²	
Bending Stress	fb	146	N/mm ²	
Allowables				
Yield Stress	Fy	250	N/mm ²	
Buckling Critical Stress	Fc	200	N/mm ²	
Bending Modulus of Rupture Stress	Fb	285	N/mm ²	



Combined Compression and Bending Interaction

Axial Stress Ratio	Ra	0.19	Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.51	Bruhn C4.12, use rupture allowable Fb
Margin of Safety	MS	0.14	Must be greater than zero, includes the factor of safety

Corner Post Insert Analysis - Insert is subject to pure bending.					
Bending Stress	fb	209	N/mm²	The bending stress at the bottom of the post	
Bending Modulus of Rupture Stress	Fb	400	N/mm ²	Assume Ftu for bending failure	
Margin of Safety	MS	0.53		Must be greater than zero, includes the factor of safety	

Corner Post Footing Analysis

Insert Type	Cast-In-Place Concrete			
Soil description	Loose gravel, or loose sand and gravel			
Soil category	•	Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m ²	Shaft friction
Footing capability	Pfooting	106814 10892	N	
		10092	kg	
Maximum compression load	Pcomp	8274	kg	
Ratio to Requirement	RtoR	1.32		Must be greater than 1.0

Corner Post (TP)

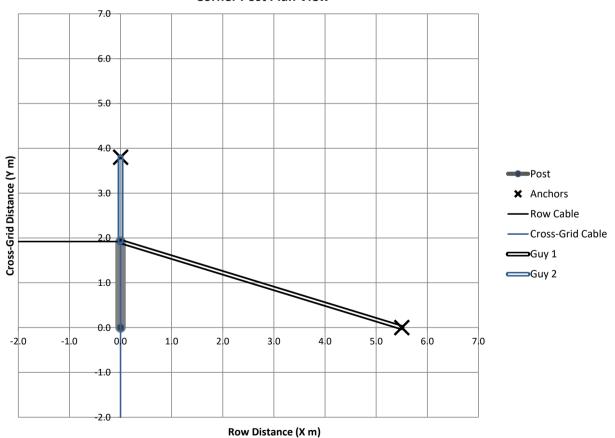
1759-CR01_P&T_Marciano_StructType_27May25

Corner posts are sized using the maximum wind loadings (roof and wall net loadings). Hail loading is considered minimal on a corner post. The analysis below assesses the anchor loadings based on no moment at the base of the corner post. In reality, a moment will exist but this will not have a significant impact on guy and cable forces. However it will have a significant impact on the post stress, and therefore is included in the stress calculations below.

Inputs

Description	Variable	Value	Units	Comments
Select Main Post Material	125NB Medium / Grade 250			D _{WB_Top_Row} T _{Cable Max C6}
Outside Diameter	D	139.7	mm	Cable_Max_CG
Wall Thickness	t	5.0	mm	
Cross Sectional Area	Α	2116	mm^2	D _{WB_Top_CG} T _{G1} T _{Cable_Max_Row}
2nd Moment of Area	1	4805412	mm^4	
Elastic Modulus	E	207000	N/mm ²	$/T_{G2}$
Yield Strength	Fy	250	N/mm ²	// 62 \\
Tensile Strength	Ft	320	N/mm ²	
Buckling Strength	Fc	200	N/mm ²	$A_1 \bullet \downarrow^{\theta_{G1}} \theta_{P1}$
Select Insert Material	100NB	Heavy / Grad	le 300	L ₁
Outside Diameter	D	114.3	mm	θ_{P2}
Wall Thickness	t	5.4	mm	θ_{G2}
2nd Moment of Area	1	2745389	mm^4	L ₂
Yield Strength	Fy	300	N/mm ²	A ₂
Tensile Strength	Ft	400	N/mm ²	-

Corner Post Plan View



Corner Post Configuration

Anchor Locations	A1	5.50	0.00	(m, m) assuming post base at (0,0)
	A2	0.00	3.80	(m, m) assuming post base at (0,0)
Post Angle (Viewed from CG Direction [Y])	θ_{P1}	90	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle (Viewed from Row Direction [X])	θ_{P2}	69	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle	θ_{PMIN}	69	deg	This is the minimum angle the post makes with the ground plane
Vector on ground this is measured on		0.0	1.9	(m,m) assuming post base at (0,0)
Post Length	Lp	5.4	m	Post length above ground - these posts use an insert
Walls along <u>row ends</u> of block.		Wall o	n Guy	Only applicable if walls are present
Walls along sides of block.		Wall o	n Guy	Only applicable if walls are present

Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

Maximum Row-Cable Load	$T_{Cable_Max_Row}$	4907	kg	
Maximum Cross-Grid Cable Load	$T_{Cable_Max_CG}$	4111	kg	
Percentage of perimeter cable load (Row) Percentage of perimeter cable load (CG)		70% 70%		The perimeter cables only carry 50% of the aerodynamic load compared to the interior cables. To account for other
Wall Net Loading applied to Top of CP (X Dir)		548	kg	variations, this is increased to 70%.
Wall Net Loading applied to Top of CP (Y Dir)		438	kg	
Wall Tension Loading applied to CP (X Dir)		153	kg	
Wall Tension Loading applied to CP (Y Dir)		153	kg	
Corner Post Load (Row)	т	4136	kg	
Corrier Post Load (Now)	T _{CP_Row}	4130	ĸg	
Corner Post Load (CG)	T_{CP_CG}	3468	kg	

The above forces act at the top of the post. The post remains in static equilibrium, and therefore the guy forces can be computed from the sum of the forces in 3 dimensions.

Guy 1 Load	T_{G1}	5773	kg	
Guy 2 Load	T_{G2}	4876	kg	
Maximum Guy Load	T_{G_Max}	5773	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	8916	kg	The maximum load at any part of the column
Post Length	Lp	5.4	m	Post length above ground - these posts use an insert
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δу_рр	50	mm	Must get the final position of the post top within this
Equivalent lateral load due this deflection	Ру	971	N	
Bending moment due this lateral load	M1	5201825	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	4371698	Nmm	Maximum at bottom of post, assuming a square root distribution.
Combined wall net loadings	M3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height.
Stress Calculations				
Axial Stress	fa	41	N/mm ²	
Bending Stress	fb	139	N/mm²	
<u>Allowables</u>				
Yield Stress	Fy	250	N/mm ²	
Buckling Critical Stress	Fc	200	N/mm ²	
Bending Modulus of Rupture Stress	Fb	285	N/mm ²	



Combined Compression and Bending	Interaction
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Margin of Safety	MS	0.15	Must be greater than zero, includes the factor of safety
Bending Stress Ratio	Rb	0.49	Bruhn C4.12, use rupture allowable Fb
Axial Stress Ratio	Ra	0.21	Bruhn C4.12, use minimum of Fc or Fy

Corner Post Insert Analysis - Insert is subject to pure bending.							
Bending Stress Bending Modulus of Rupture Stress	fb Fb	199 400	N/mm ² The bending stress at the bottom of the post N/mm ² Assume Ftu for bending failure				
Margin of Safety	MS	0.61	Must be greater than zero, includes the factor of safety				

Corner Post Footing Analysis

Insert Type	Cast-In-Place Concrete			
Soil description	Loose gravel, or	loose sand and	gravel	1
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m ²	Shaft friction
Footing capability	Pfooting	106814	N	
		10892	kg	
Maximum compression load	Pcomp	8916	kg	
Ratio to Requirement	RtoR	1.22		Must be greater than 1.0

Corner Post (Angled)

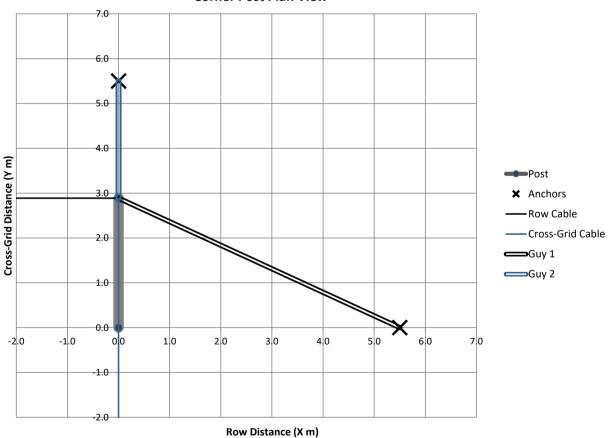
1759-CR01_P&T_Marciano_StructType_27May25

Corner posts are sized using the maximum wind loadings (roof and wall net loadings). Hail loading is considered minimal on a corner post. The analysis below assesses the anchor loadings based on no moment at the base of the corner post. In reality, a moment will exist but this will not have a significant impact on guy and cable forces. However it will have a significant impact on the post stress, and therefore is included in the stress calculations below.

Inputs

Description	Variable	Value	Units	Comments
Select Main Post Material	125NB M	1edium / Gra	de 250	D _{WB_Top_Row} T _{Cable Max C6}
Outside Diameter	D	139.7	mm	Cable_Max_CG
Wall Thickness	t	5.0	mm	
Cross Sectional Area	Α	2116	mm^2	D _{WB_Top_CG} T _{G1} T _{Cable_Max_Row}
2nd Moment of Area	1	4805412	mm^4	
Elastic Modulus	E	207000	N/mm ²	$/T_{G2}$
Yield Strength	Fy	250	N/mm ²	// 62 \\
Tensile Strength	Ft	320	N/mm ²	
Buckling Strength	Fc	196	N/mm ²	$A_1 \bullet \downarrow^{\theta_{G1}} \theta_{P1}$
Select Insert Material	100NB	Heavy / Grad	le 300	L ₁
Outside Diameter	D	114.3	mm	θ_{P2}
Wall Thickness	t	5.4	mm	θ_{G2}
2nd Moment of Area	1	2745389	mm^4	L ₂
Yield Strength	Fy	300	N/mm ²	A ₂
Tensile Strength	Ft	400	N/mm ²	-

Corner Post Plan View



Corner Post Configuration

Anchor Locations	A1	5.50	0.00	(m, m) assuming post base at (0,0)
	A2	0.00	5.50	(m, m) assuming post base at (0,0)
Post Angle (Viewed from CG Direction [Y])	θ_{P1}	90	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle (Viewed from Row Direction [X])	θ_{P2}	60	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle	θ_{PMIN}	60	deg	This is the minimum angle the post makes with the ground plane
Vector on ground this is measured on		0.0	2.9	(m,m) assuming post base at (0,0)
Post Length	Lp	5.8	m	Post length above ground - these posts use an insert
Walls along row ends of block.		Wall o	n Guy	Only applicable if walls are present
Walls along sides of block.		Wall	n Guy	Only applicable if walls are present

Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

Maximum Row-Cable Load	$T_{Cable_Max_Row}$	4907	kg	
Maximum Cross-Grid Cable Load	$T_{Cable_Max_CG}$	4111	kg	
Percentage of perimeter cable load (Row) Percentage of perimeter cable load (CG)		70% 70%		The perimeter cables only carry 50% of the aerodynamic load compared to the interior cables. To account for other
Wall Net Loading applied to Top of CP (X Dir)		548	kg	variations, this is increased to 70%.
Wall Net Loading applied to Top of CP (Y Dir)		438	kg	
Wall Tension Loading applied to CP (X Dir)		153	kg	
Wall Tension Loading applied to CP (Y Dir)		153	kg	
Corner Post Load (Row)	т	4136	kg	
Corrier Post Load (Now)	T _{CP_Row}	4130	ĸg	
Corner Post Load (CG)	T_{CP_CG}	3468	kg	

The above forces act at the top of the post. The post remains in static equilibrium, and therefore the guy forces can be computed from the sum of the forces in 3 dimensions.

Guy 1 Load	T_{G1}	5996	kg	
Guy 2 Load	T_{G2}	3558	kg	
Maximum Guy Load	T_{G_Max}	5996	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	7982	kg	The maximum load at any part of the column
Post Length	Lp	5.8	m	Post length above ground - these posts use an insert
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δу_рр	50	mm	Must get the final position of the post top within this
Equivalent lateral load due this deflection	Ру	775	Ν	
Bending moment due this lateral load	M1	4476242	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	3914047	Nmm	Maximum at bottom of post, assuming a square root distribution.
Combined wall net loadings	М3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height.
Stress Calculations				
Axial Stress	fa	37	N/mm ²	
Bending Stress	fb	122	N/mm ²	
<u>Allowables</u>				
Yield Stress	Fy	250	N/mm ²	
Buckling Critical Stress	Fc	196	N/mm ²	
Bending Modulus of Rupture Stress	Fb	285	N/mm ²	

Combined Compression and Bending Interaction

Axial Stress Ratio	Ra	0.19	Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.43	Bruhn C4.12, use rupture allowable Fb
-			
Margin of Safety	MS	0.30	Must be greater than zero, includes the factor of safety

Corner Post Insert Analysis - Insert is subject to pure bending.						
Bending Stress	fb	175	N/mm²	The bending stress at the bottom of the post		
Bending Modulus of Rupture Stress	Fb	400	N/mm ²	Assume Ftu for bending failure		
Margin of Safety	MS	0.83		Must be greater than zero, includes the factor of safety		

Corner Post Footing Analysis

Insert Type	Cast-In-Place Co	oncrete		
Soil description	Loose gravel, or loose sand and gravel			
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" \times "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m ²	Shaft friction
Footing capability	Pfooting	106814	N	
		10892	kg	
Maximum compression load	Pcomp	7982	kg	
Ratio to Requirement	RtoR	1.36		Must be greater than 1.0



Corner Post (55deg)

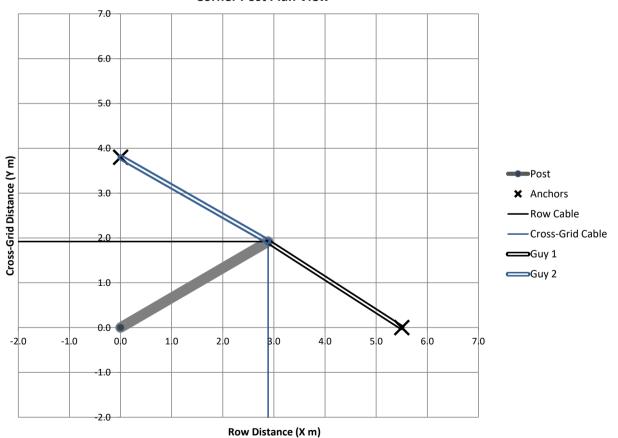
1759-CR01_P&T_Marciano_StructType_27May25

Corner posts are sized using the maximum wind loadings (roof and wall net loadings). Hail loading is considered minimal on a corner post. The analysis below assesses the anchor loadings based on no moment at the base of the corner post. In reality, a moment will exist but this will not have a significant impact on guy and cable forces. However it will have a significant impact on the post stress, and therefore is included in the stress calculations below.

Inputs

Description	Variable	Value	Units	Comments
Select Main Post Material	125NB N	1edium / Gra	de 250	D _{WB_Top_Row} T _{Cable Max C6}
Outside Diameter	D	139.7	mm	Cable_Max_CG
Wall Thickness	t	5.0	mm	
Cross Sectional Area	Α	2116	mm^2	D _{WB_Top_CG} T _{G1} T _{Cable_Max_Row}
2nd Moment of Area	1	4805412	mm^4	
Elastic Modulus	Е	207000	N/mm ²	$/T_{G2}$
Yield Strength	Fy	250	N/mm ²	/ / 62 \
Tensile Strength	Ft	320	N/mm ²	
Buckling Strength	Fc	177	N/mm ²	$A_1 \bullet \theta_{P1}$
Select Insert Material	100NB	Heavy / Grad	le 300	L ₁
Outside Diameter	D	114.3	mm	θ_{P2}
Wall Thickness	t	5.4	mm	θ_{G2}
2nd Moment of Area	1	2745389	mm^4	L ₂
Yield Strength	Fy	300	N/mm ²	A_2
Tensile Strength	Ft	400	N/mm ²	-

Corner Post Plan View



Corner Post Configuration

Anchor Locations	A1	5.50	0.00	(m, m) assuming post base at (0,0)
	A2	0.00	3.80	(m, m) assuming post base at (0,0)
Post Angle (Viewed from CG Direction [Y])	θ_{P1}	60	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle (Viewed from Row Direction [X])	θ_{P2}	69	deg	90 deg for vertical, 60 deg for a 60deg post
Post Angle	θ_{PMIN}	55	deg	This is the minimum angle the post makes with the ground _plane
Vector on ground this is measured on		2.9	1.9	(m,m) assuming post base at (0,0)
Post Length	Lp	6.1	m	Post length above ground - these posts use an insert
Walls along <u>row ends</u> of block.		Wall on Guy		Only applicable if walls are present
Walls along sides of block.		Wall	n Guy	Only applicable if walls are present

Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

Maximum Row-Cable Load	$T_{Cable_Max_Row}$	4907	kg	
Maximum Cross-Grid Cable Load	$T_{Cable_Max_CG}$	4111	kg	
Percentage of perimeter cable load (Row)		70%		The perimeter cables only carry 50% of the aerodynamic load compared to the interior cables. To account for other
Percentage of perimeter cable load (CG)		70%		variations, this is increased to 70%.
Wall Net Loading applied to Top of CP (X Dir)		548	kg	
Wall Net Loading applied to Top of CP (Y Dir)		438	kg	
Wall Tension Loading applied to CP (X Dir)		153	kg	
Wall Tension Loading applied to CP (Y Dir)		153	kg	
Corner Post Load (Row)	т	4136	kg	
Corrier Post Load (Now)	T_{CP_Row}	4130	κg	
Corner Post Load (CG)	T_{CP_CG}	3468	kg	

The above forces act at the top of the post. The post remains in static equilibrium, and therefore the guy forces can be computed from the sum of the forces in 3 dimensions.

Guy 1 Load	T_{G1}	4481	kg	
Guy 2 Load	T_{G2}	5542	kg	
Maximum Guy Load	T_{G_Max}	5542	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	10128	kg	The maximum load at any part of the column
Post Length	Lp	6.1	m	Post length above ground - these posts use an insert
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δу_рр	50	mm	Must get the final position of the post top within this
Equivalent lateral load due this deflection	Ру	663	N	
Bending moment due this lateral load	M1	4030785	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	4966303	Nmm	Maximum at bottom of post, assuming a square root distribution.
Combined wall net loadings	М3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height.
Stress Calculations				
Axial Stress	fa	47	N/mm ²	
Bending Stress	fb	131	N/mm²	
Allowables				
Yield Stress	Fy	250	N/mm ²	
Buckling Critical Stress	Fc	177	N/mm ²	
Bending Modulus of Rupture Stress	Fb	285	N/mm ²	



Combined Compression and Bending Interaction

Axial Stress Ratio	Ra	0.27	Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.46	Bruhn C4.12, use rupture allowable Fb
· ·			
Margin of Safety	MS	0.10	Must be greater than zero, includes the factor of safety

Corner Post Insert Analysis - Insert is subject to pure bending.						
Bending Stress	fb	187	N/mm ² The bending stress at t	he bottom of the post		
Bending Modulus of Rupture Stress	Fb	400	N/mm ² Assume Ftu for bendin	g failure		
Margin of Safety	MS	0.71	Must be greater than a	ero, includes the factor of safety		

Corner Post Footing Analysis

Insert Type	Cast-In-Place Co	oncrete		
Soil description	Loose gravel, or	loose sand and	gravel	
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m ²	Shaft friction
Footing capability	Pfooting	106814	N	
		10892	kg	
Maximum compression load	Pcomp	10128	kg	
Ratio to Requirement	RtoR	1.08		Must be greater than 1.0

Perimeter Breaker Post (SE)

1759-CR01_P&T_Marciano_StructType_27May25

Breaker posts are used to break up large structures into smaller blocks. If a failure were to occur on one side of the breaker post, the breaker posts prevents the failure cascading into the other side. Perimeter breaker posts are those breaker posts located on the perimeter of a large structure. Given a failure on one side of the structure, the perimeter breaker post effectively becomes a corner post for the opposing side of the structure. When subject to severe wind and hail, the perimeter breaker posts effectively acts like a corner post in one direction and a regular perimeter post in the other direction. The analysis below sizes the post in accordance with this loading.

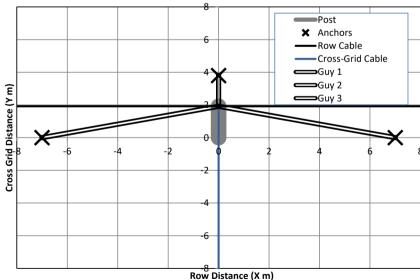
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Description	Variable	Value	Units	Comments
Select Main Post Material	125NB	Medium / Gra	ade 350]
Outside Diameter	D	139.7	mm	T_{Cable3} T_{Cable2}
Wall Thickness	t	5.0	mm	Cable2
Cross Sectional Area	Α	2116	mm^2	
2nd Moment of Area	1	4805412	mm^4	T_{G1} T_{Cable1}
Elastic Modulus	Ε	207000	N/mm ²	Cable1
Yield Strength	Fy	350	N/mm ²	$D_{WB} = T_{G2}$
Tensile Strength	Ft	430	N/mm ²	D_{WB}
Buckling Strength	Fc	228	N/mm ²	/
				$A_1 \bullet \theta_{G1} \theta_{P1} \bullet$
Select Insert Material	100NE	Heavy / Grad	de 300	opi.
Outside Diameter	D	114.3	mm	L ₁
Wall Thickness	t	5.4	mm	θ_{P2}
2nd Moment of Area	1	2745389	mm^4	θ_{62}
Yield Strength	Fy	300	N/mm ²	L ₂
Tensile Strength	Ft	400	N/mm ²	A_2 A_3

Perimeter Breaker Post Configuration

Perimeter Breaker Post Orientation		Row	Cable	Normally PBP used for breaking row cables
Post Angle	θ_{P}	69	deg	90 deg for vertical PBP, 60 deg for a 60deg PBP
Anchor Locations A1 and A3	A1, A3	7.0	m	Distance from post base
Anchor Location A2 (Double Anchor & Guy)	A2	3.8	m	Distance from post base
Wall Net Configuration		Wall o	n Guy	

Perimeter Breaker Post Plan View



Determination of Guy Forces

Maximum Row-Cable Load	$T_{Cable_Max_Row}$	4907	kg	Maximum cable loadings as obtained from "Cables" Worksheet. The CG load is conservatively increased by
Maximum Cross-Grid Cable Load	T _{Cable_Max_CG}	4933	kg	120% to account for two different shorter CG cables terminating at this post.
Wall Netting Top of Post Loading (Row)	D _{WB_Top_Row}	0	kg	
Wall Netting Top of Post Loading (Cross-Grid)	D _{WB_Top_CG}	876	kg	Drag force component that applies at the top of the post
Percentage of maximum cable load	W5_10F_CC	70%	Ü	The perimeter cables only carry 50% of the aerodynamic load compared to the interior cables. To account for other variations, this is increased to 70%.
Perimeter Breaker Post Load (Row)	T_{CP_Row}	3435	kg	Combination of the elevated cable forces and any forces
Perimeter Breaker Post Load (CG)	T _{CP_CG}	5809	kg	due to wall net loadings
The above forces act at the top of the post. The pof the forces in 3 dimensions.	ost remains in s	static equilib	rium, and t	herefore the guy forces can be computed from the sum
Guy 1 Load	T_{G1}	4325	kg	Obtained from simultaneous equations with post in static
Guy 2 Load (2 Anchors)	T_{G2}	4083	kg	equilibrium.
Guy 3 Load	T_{G3}	0	kg	The third guy is assumed to become unloaded when opposing guy (G1) becomes fully loaded.
Maximum Guy Load	T_{G_Max}	4325	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	10816	kg	The maximum load at any part of the column
Post Length	Lp	5.4	m	Post length above ground - these posts use an insert
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	dy_pp	50	mm	The post must be set straight on installation. In practise this cannot be achieved, so it is assumed that the post top
Equivalent lateral load due this deflection	Ру	971	N	is displaced the following amount.
Bending moment due to the lateral load	M1	5201825	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	5303207	Nmm	Maximum at bottom of post, assuming a square root distribution.
Bending moment due to wall net loading	M3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height. Only applicable if a wall net is attached to the post.
Stress Calculations				
Axial Stress	fa	50	N/mm ²	Based on the post compression found above.
Bending Stress	fb	153	N/mm ²	Obtained from the maximum of (M1+M2) at bottom of post or (M3+0.5*M1+0.7071*M2) at middle of post.
<u>Allowables</u>				
Yield Stress	Fy	350	N/mm ²	
Buckling Critical Stress	Fc	228	N/mm ²	
Bending Modulus of Rupture Stress	Fb	390	N/mm ²	
Combined Compression and Bending Interaction	L			
Axial Stress Ratio	Ra	0.22		Bruhn C4.12, use minimum of Fc or Fy
				_ , _ , _ , _ , _ , _ , _ , _ , _ , _ ,



Bending Stress Ratio

Margin of Safety (Post)

Rb

MS

0.39

0.31

Bruhn C4.12, use rupture allowable Fb

Must be greater than zero, includes the factor of safety

Perimeter Breaker Post Insert Analysis - Insert is subject to pure bending.						
			. 2			
Bending Stress	fb	219	N/mm²	The bending stress at the bottom of the post		
Bending Modulus of Rupture Stress	Fb	400	N/mm ²	Assume Ftu for bending failure		
Margin of Safety	MS	0.46		Must be greater than zero, includes the factor of safety		

Perimeter Breaker Post Footing Analysis

Insert Type	Cast-In-Place Concrete]
Soil description	Loose gravel, or loose sand and gravel			
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m ²	Shaft friction
Footing capability	Pfooting	106814	N	
		10892	kg	
Maximum compression load	Pcomp	10816	kg	
Ratio to Requirement	RtoR	1.01		Must be greater than 1.0

Perimeter Breaker Post

1759-CR01_P&T_Marciano_StructType_27May25

Breaker posts are used to break up large structures into smaller blocks. If a failure were to occur on one side of the breaker post, the breaker posts prevents the failure cascading into the other side. Perimeter breaker posts are those breaker posts located on the perimeter of a large structure. Given a failure on one side of the structure, the perimeter breaker post effectively becomes a corner post for the opposing side of the structure. When subject to severe wind and hail, the perimeter breaker posts effectively acts like a corner post in one direction and a regular perimeter post in the other direction. The analysis below sizes the post in accordance with this loading.

n		

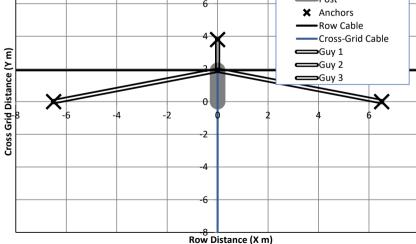
Description	Variable	Value	Units	Comments
Select Main Post Material	125NB Medium / Grade 250			1
Outside Diameter	D	139.7	mm	T _{Cable3} T _{Cable3}
Wall Thickness	t	5.0	mm	Cable3 T _{Cable2}
Cross Sectional Area	Α	2116	mm^2	
2nd Moment of Area	1	4805412	mm^4	T _{G1} T _{Coblet}
Elastic Modulus	Е	207000	N/mm ²	T _{Cable1}
Yield Strength	Fy	250	N/mm ²	D_{WB} T_{G2}
Tensile Strength	Ft	320	N/mm ²	D_{WB} $//T_{G2}$
Buckling Strength	Fc	200	N/mm ²	/
				$A_1 \bigoplus_{\theta_{G1}} \theta_{\theta_{P1}}$
Select Insert Material	100NE	Heavy / Grad	de 300	ОРІ
Outside Diameter	D	114.3	mm	L ₁
Wall Thickness	t	5.4	mm	θ_{P2}
2nd Moment of Area	1	2745389	mm^4	θ_{G2}
Yield Strength	Fy	300	N/mm ²	L ₂
Tensile Strength	Ft	400	N/mm ²	A_2 A_3

Perimeter Breaker Post Configuration

Perimeter Breaker Post Orientation		Row	Cable	Normally PBP used for breaking row cables
Post Angle	$\theta_{ t P}$	69	deg	90 deg for vertical PBP, 60 deg for a 60deg PBP
Anchor Locations A1 and A3	A1, A3	6.5	m	Distance from post base
Anchor Location A2 (Double Anchor & Guy)	A2	3.8	m	Distance from post base
Wall Net Configuration		Wall on Guy		

Post * Anchors Row Cable

Perimeter Breaker Post Plan View



Determination of Guy Forces

Maximum Row-Cable Load	$T_{Cable_Max_Row}$	4907	kg	Maximum cable loadings as obtained from "Cables"
Maximum Cross-Grid Cable Load	$T_{Cable_Max_CG}$	4111	kg	Worksheet
Wall Netting Top of Post Loading (Row)	$D_{WB_Top_Row}$	0	kg	Drag force component that applies at the top of the post
Wall Netting Top of Post Loading (Cross-Grid)	$D_{WB_Top_CG}$	876	kg	Drug force component that applies at the top of the post
Percentage of maximum cable load		70%		The perimeter cables only carry 50% of the aerodynamic load compared to the interior cables. To account for other variations, this is increased to 70%.
Perimeter Breaker Post Load (Row)	T_{CP_Row}	3435	kg	Combination of the elevated cable forces and any forces
Perimeter Breaker Post Load (CG)	T_{CP_CG}	4987	kg	due to wall net loadings

The above forces act at the top of the post. The post remains in static equilibrium, and therefore the guy forces can be computed from the sum of the forces in 3 dimensions.

Guy 1 Load	T_{G1}	4451	kg	Obtained from simultaneous equations with post in static
Guy 2 Load (2 Anchors)	T_{G2}	3505	kg	equilibrium.
Guy 3 Load	T_{G3}	0	kg	The third guy is assumed to become unloaded when opposing guy (G1) becomes fully loaded.
Maximum Guy Load	T_{G_Max}	4451	kg	Note guys evaluated under "Guys" worksheet
Post Compression	Pcomp	9859	kg	The maximum load at any part of the column
Post Length	Lp	5.4	m	Post length above ground - these posts use an insert

Bending Moment due to Lateral Deflection

Maximum lateral deflection after post setting	dy_pp	50	mm	The post must be set straight on installation. In practise this cannot be achieved, so it is assumed that the post top
Equivalent lateral load due this deflection	Ру	971	N	is displaced the following amount.
Bending moment due to the lateral load	M1	5201825	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	4834106	Nmm	Maximum at bottom of post, assuming a square root distribution. Maximum at the centre of the post, assuming a quadratic
Bending moment due to wall net loading	M3	0	Nmm	distribution over post height. Only applicable if a wall net is attached to the post.

Stress Calculations

Buckling Critical Stress

Axial Stress Ratio

Bending Modulus of Rupture Stress

Axial Stress	fa	46	N/mm ²	Based on the post compression found above.
Bending Stress	fb	146	N/mm²	Obtained from the maximum of (M1+M2) at bottom of post or (M3+0.5*M1+0.7071*M2) at middle of post.
<u>Allowables</u>				
Yield Stress	Fy	250	N/mm ²	

200

285

0.23

N/mm²

N/mm²

Bruhn C4.12, use minimum of Fc or Fy

Fc

Fb

Ra

Combined Compression and Bending Interaction

Margin of Cafety (Post)	MC	0.00	Must be greater than zero, includes the factor of safety
Bending Stress Ratio	Rb	0.51	Bruhn C4.12, use rupture allowable Fb

Must be greater than zero, includes the factor of safety Margin of Safety (Post) MS 0.08



Perimeter Breaker Post Insert Analysis - Insert is subject to pure bending.						
Bending Stress	fb	209	N/mm ²	The bending stress at the bottom of the post		
Bending Modulus of Rupture Stress	Fb	400	N/mm²	Assume Ftu for bending failure		
Margin of Safety	MS	0.53		Must be greater than zero, includes the factor of safety		

Perimeter Breaker Post Footing Analysis

Insert Type	Cast-In-Place Co	oncrete]
Soil description	Loose gravel, or	r loose sand and	gravel	
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter / width	d	0.68	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.80	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.36	m^2	
Footing shaft area	As	1.71	m^2	Shaft friction
Footing capability	Pfooting	106814	N	
		10892	kg	
Maximum compression load	Pcomp	9859	kg	
Ratio to Requirement	RtoR	1.10		Must be greater than 1.0



Interior Breaker Post

1759-CR01_P&T_Marciano_StructType_27May25

Comments

Breaker posts are used to break up large structures into smaller blocks. If a failure were to occur on one side of the breaker post, the breaker posts prevents the failure cascading into the other side. Interior breaker posts are those breaker posts located on the interior of a large structure, normally situated between perimeter breaker posts and located on row direction cable lines. Given a failure on one side of the structure, the interior breaker post effectively becomes a perimeter post for the opposing side of the structure.

iliputs			
Description	Variable	Value	Units
Select Main Post Material	125NB	Medium / Gra	ade 250
Outside Diameter	D	139.7	mm
Wall Thickness	t	5.0	mm
Cross Sectional Area	Α	2116	mm^2
2nd Moment of Area	1	4805412	mm^4
Elastic Modulus	Е	207000	N/mm ²
Yield Strength	Fy	250	N/mm ²
Tensile Strength	Ft	320	N/mm ²
Buckling Strength	Fc	200	N/mm ²
Select Insert Material	100NB	Heavy / Gra	de 300
Outside Diameter	D	114.3	mm
Wall Thickness	t	5.4	mm
2nd Moment of Area	1	2745389	mm^4
Yield Strength	Fy	300	N/mm ²

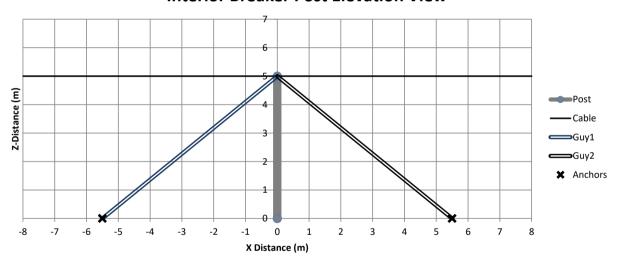
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Interior Breaker Post Elevation View

N/mm²

400

Ft



Interior Breaker Post Configuration

Interior Breaker Post Orientation Anchor Placement Distance

Tensile Strength

Row 5.5

Cable m

Normally IBP used for breaking row cables Anchor placement distance from base of post

Axial Compression due Guys

Guy 1				
Maximum Cable Load due Wind & Hail	T_Max	4907	kg	Maximum cable loadings as obtained from "Cables" Worksheet
Guy wire angle	θ_{G1}	42.3	deg	No. in the contract of the con
Guy load	T_{G1}	6632	kg	
Guy 2				
Cable Load due Hail on no pre-tension cable	T_{Max}	1500	kg	The other cable on opposing side unloads to zero, but for conservatism it is assumed the other side stays at its initial pre-tension.
Guy wire angle	θ_{G2}	42.3	deg	Guy Angle
Guy load	T_{G2}	2027	kg	
Maximum Guy Load	T_{G_Max}	6632	kg	Note guys evaluated under "Guys" worksheet
Post Length	Lp	5.0	m	
Post Compression	Pc	5825	kg	The maximum load at any part of the column
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δу_рр	50.0	mm	The post must be set straight on installation. In practise this cannot be achieved, so it is assumed that the post top is
Equivalent lateral load due this deflection	Ру	1194	N	displaced the following amount.
Bending moment due this lateral load	M1	5968322	Nmm	Maximum at base of post, linear relationship.
Secondary moment due compression	M2	2856092	Nmm	Maximum at bottom of post.
Stress Calculations				
Axial Stress	fa	27	N/mm²	Axial stress due compression
Bending Stress	fb	128	N/mm ²	Bending stress due to the moment (M1 + M2)
Allowables				
Yield Stress	Fy	250	N/mm ²	
Buckling Critical Stress	Fc	200	N/mm ²	
Bending Modulus of Rupture Stress	Fb	285	N/mm ²	
Combined Compression and Bending Interaction				
Axial Stress Ratio	Ra	0.13		Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.45		Bruhn C4.12, use rupture allowable Fb
Margin of Safety	MS	0.37		Must be greater than zero, includes the factor of safety
Interior Breaker Post Insert Analysis - Insert is	subject to	pure bending	J .	
Danding Chases	£ı_	104	N./ 2	The bonding stores at the best, and Citizens
Bending Stress	fb	184	N/mm ²	The bending stress at the bottom of the post
Bending Modulus of Rupture Stress	Fb	400	N/mm ²	Assume Ftu for bending failure
Margin of Safety	MS	0.74		Must be greater than zero, includes the factor of safety



Interior Breaker Post Footing Analysis

Insert Type	Rammed Inser	rt		
Soil description	Loose gravel, o	or loose sand a	nd gravel	
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter	d	0.53	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.90	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.27	m^2	
Footing shaft area	As	0.39	m ²	Shaft friction
Footing capability	Pfooting	61014	N	
		6222	kg	
Maximum compression load	Pcomp	5825	kg	
Ratio to Requirement	RtoR	1.07		Must be greater than 1.0

Perimeter Post (TP)

1759-CR01_P&T_Marciano_StructType_27May25

Perimeter posts are sized using the maximum wind loadings (roof and wall nets loadings). This conservative method assumes all wind loading along the longest cross-grid or row run is all taken by that cable run. This ignores the assistance provided by interior posts and perpendicular cable runs.

Inputs

Description	Variable	Value	Units	Comments
				-
Select Main Post Material	100NB Light / Grade 350			
Outside Diameter	D	114.3	mm	
Wall Thickness	t	3.6	mm	T_{Cable} $D_{WB_Top_CG}$
Cross Sectional Area	Α	1252	mm^2	Cable - WB_Top_CG (If Applic.)
2nd Moment of Area	I	1919837	mm^4	T_{G}
Elastic Modulus	Е	207000	N/mm ²	
Yield Strength	Fy	350	N/mm ²	
Tensile Strength	Ft	430	N/mm ²	н //
Buckling Strength	Fc	154	N/mm ²	
				_ //
Select Insert Material	90NB Heavy / Grade 300			θ_{P} θ_{G}
Outside Diameter	D	101.6	mm	
Wall Thickness	t	5.0	mm	
2nd Moment of Area	I	1774693	mm^4	
Yield Strength	Fy	300	N/mm ²	└
Tensile Strength	Ft	400	N/mm ²	

Perimeter Post Configuration

Perimeter Post Location Wall Net Configuration Anchor Placement Distance Post Angle

Post Angle Post Length Cross-Grid
No Wall

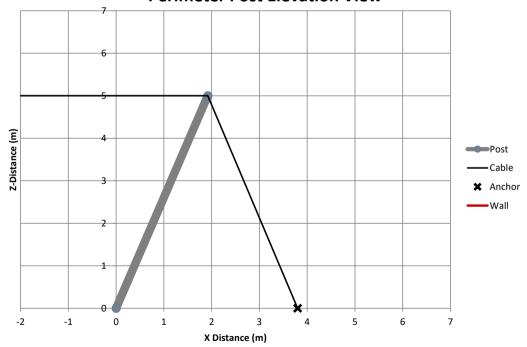
3.8
Distance from post base
69
deg
90 deg for vertical, 60 deg for a 60deg post
5.4
m Post length above ground - these posts use an insert

Perimeter Post Elevation View

L

 θ_{P}

Lp



Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

				Obtained from Anchor worksheet, depends on perimeter			
Maximum Cable Load	T_{Cable}	4111	kg	post locations. Based on maximum aerodynamic forces			
Maximum Wall Loading	T_{Wall}	0	kg	Assumes 11/18 of the wall net loading ends up at the top of the post (if applicable)			
Total Load at Top of Post	T_Total	4111	kg	Combined Cable & Wall Loading			
Guy wire angle	θ_{G}	69.4	deg	Reference to the ground plane.			
Maximum Guy load	T_{G_Max}	5780	kg	Note guys evaluated under "Guys" worksheet			
Pole Compression	P_{comp}	5794	kg	The maximum load at any part of the column			
_ , , , , , , , , , , , , , , , , , , ,							
Bending Moment due to Lateral Deflection							
Maximum lateral deflection after post setting	δy_pp	50.0	mm	ine post must be set straignt on installation. In practise			
Equivalent lateral load due this deflection	Py	388	N	this cannot be achieved, so it is assumed that the post top is			
Bending moment due this lateral load	M1	2078210	Nmm	displaced the following amount Maximum at base of post, linear distribution.			
Secondary moment due compression	M2	2841156	Nmm	Maximum at bottom of post, assuming a square root			
Secondary moment due compression	1412	2041130	14111111	distribution.			
Bending moment due wall net loading	М3	0	Nmm	Maximum at the centre of the post, assuming a quadratic distribution over post height. Only applicable if a wall net is attached to the post.			
Stress Calculations							
Axial Stress	fa	45	N/mm ²	Based on the post compression found above.			
Bending Stress	fb	146	N/mm²	Obtained from the maximum of (M1+M2) at bottom of post or (M3+0.5*M1+0.7071*M2) at middle of post.			
<u>Allowables</u>							
Yield Stress	Fy	350	N/mm ²				
Critical Buckling Stress	Fc	154	N/mm ²				
Bending Modulus of Rupture Stress	Fb	430	N/mm ²				
Combined Compression and Bending Interaction							
Axial Stress Ratio	Ra	0.29		Bruhn C4.12, use minimum of Fc or Fy			
Bending Stress Ratio	Rb	0.34		Bruhn C4.12, use rupture allowable Fb			
Margin of Safety	MS	0.26		Must be greater than zero, includes the factor of safety			
Perimeter Post Insert Analysis - Insert is subject to pure bending.							
Bending Stress	fb	141	N/mm ²	The bending stress at the bottom of the post			
Bending Modulus of Rupture Stress	Fb	400	N/mm²	Assume Ftu for bending failure			
Margin of Safety	MS	1.27		Must be greater than zero, includes the factor of safety			

Perimeter Post Footing Analysis

Insert Type	Rammed Inse	rt		
Soil description	Loose gravel,	or loose sand an	d gravel	
Soil category		Non-cohesive	soils	
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter	d	0.53	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.90	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.27	m^2	
Footing shaft area	As	0.32	m^2	Shaft friction
Footing capability	P_{footing}	60591	N	
		6179	kg	
Maximum compression load	P_{comp}	5794	kg	
Ratio to Requirement	RtoR	1.07		To remain stable on the ground when subject to the worst combination loading from wind and hail, it is preferable to have this ratio greater than 1.0.

Perimeter Post (CG 69deg)

1759-CR01_P&T_Marciano_StructType_27May25

Perimeter posts are sized using the maximum wind loadings (roof and wall nets loadings). This conservative method assumes all wind loading along the longest cross-grid or row run is all taken by that cable run. This ignores the assistance provided by interior posts and perpendicular cable runs.

Inputs

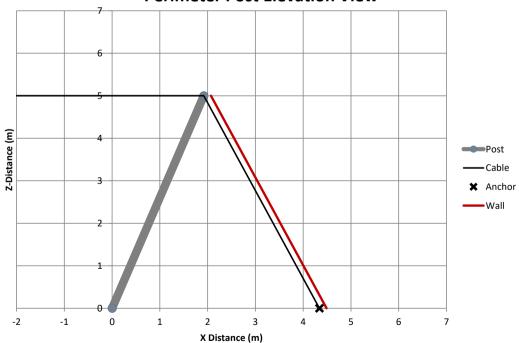
Description	Variable	Value	Units	Comments
				-
Select Main Post Material	100N	B Light / Grad	le 350	
Outside Diameter	D	114.3	mm	
Wall Thickness	t	3.6	mm	T_{Cable} $D_{WB_Top_CG}$
Cross Sectional Area	Α	1252	mm^2	Cable - WB_Top_CG (If Applic.)
2nd Moment of Area	1	1919837	mm^4	T_{G}
Elastic Modulus	Е	207000	N/mm ²	
Yield Strength	Fy	350	N/mm ²	
Tensile Strength	Ft	430	N/mm ²	н
Buckling Strength	Fc	154	N/mm ²	
				_ //
Select Insert Material	90NB	Heavy / Grad	le 300	θ_{P} θ_{G}
Outside Diameter	D	101.6	mm	
Wall Thickness	t	5.0	mm	
2nd Moment of Area	I	1774693	mm^4	
Yield Strength	Fy	300	N/mm ²	└
Tensile Strength	Ft	400	N/mm ²	

Perimeter Post Configuration

Perimeter Post Location Wall Net Configuration Anchor Placement Distance Post Angle

Post Length

Perimeter Post Elevation View



Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

Maximum Cable Load	T_Cable	4111	kg	Obtained from Anchor worksheet, depends on perimeter post locations. Based on maximum aerodynamic forces
Maximum Wall Loading	T_{Wall}	876	kg	Assumes 11/18 of the wall net loading ends up at the top of the post (if applicable)
Total Load at Top of Post	T_Total	4987	kg	Combined Cable & Wall Loading
Guy wire angle	θ_{G}	64.2	deg	Reference to the ground plane.
Maximum Guy load	T_{G_Max}	6383	kg	Note guys evaluated under "Guys" worksheet
Pole Compression	P_{comp}	6154	kg	The maximum load at any part of the column
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting Equivalent lateral load due this deflection Bending moment due this lateral load	δy_pp Py M1	50.0 388 2078210	mm N Nmm	Ine post must be set straight on installation. In practise this cannot be achieved, so it is assumed that the post top is displaced the following amount Maximum at base of post, linear distribution.
Secondary moment due compression	M2	3017478	Nmm	Maximum at bottom of post, assuming a square root
Bending moment due wall net loading	М3	0	Nmm	distribution. Maximum at the centre of the post, assuming a quadratic distribution over post height. Only applicable if a wall net is attached to the post.
Stress Calculations				
Axial Stress	fa	48	N/mm²	Based on the post compression found above.
Bending Stress	fb	152	N/mm²	Obtained from the maximum of (M1+M2) at bottom of post or (M3+0.5*M1+0.7071*M2) at middle of post.
Allowables				
Yield Stress	Fy	350	N/mm ²	
Critical Buckling Stress	, Fc	154	N/mm ²	
Bending Modulus of Rupture Stress	Fb	430	N/mm²	
Combined Compression and Bending Interaction	<u>on</u>			
Axial Stress Ratio	Ra	0.31		Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.35		Bruhn C4.12, use rupture allowable Fb
Margin of Safety	MS	0.20		Must be greater than zero, includes the factor of safety
Perimeter Post Insert Analysis - Insert is subj	iect to pur	e bending.		
			-	
Bending Stress	fb	146	N/mm ²	The bending stress at the bottom of the post
Bending Modulus of Rupture Stress	Fb	400	N/mm ²	Assume Ftu for bending failure
Margin of Safety	MS	1.19		Must be greater than zero, includes the factor of safety



Perimeter Post Footing Analysis

Insert Type	Rammed Inse	rt		
Soil description	Loose gravel,	or loose sand and	d gravel	
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20 KPa		Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter	d	0.53	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.90	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.27	m^2	
Footing shaft area	As	0.32	m ²	Shaft friction
Footing capability	P_{footing}	60591	N	
		6179	kg	
Maximum compression load	P_{comp}	6154	kg	
Ratio to Requirement	RtoR	1.00		To remain stable on the ground when subject to the worst combination loading from wind and hail, it is preferable to have this ratio greater than 1.0.

Perimeter Post (RE)

1759-CR01_P&T_Marciano_StructType_27May25

Perimeter posts are sized using the maximum wind loadings (roof and wall nets loadings). This conservative method assumes all wind loading along the longest cross-grid or row run is all taken by that cable run. This ignores the assistance provided by interior posts and perpendicular cable runs.

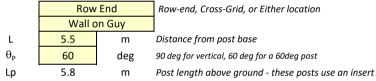
Inputs

Description	Variable	Value	Units	Comments
				7
Select Main Post Material	100N	B Light / Grad	le 350	
Outside Diameter	D	114.3	mm	4
Wall Thickness	t	3.6	mm	T_{Cable} $D_{WB_Top_CG}$
Cross Sectional Area	Α	1252	mm^2	Cable - WB_Top_CG (If Applic.)
2nd Moment of Area	I	1919837	mm^4	T_{G}
Elastic Modulus	Е	207000	N/mm ²	
Yield Strength	Fy	350	N/mm ²	
Tensile Strength	Ft	430	N/mm ²	н //
Buckling Strength	Fc	133	N/mm ²	
				_ //
Select Insert Material	90NB	Heavy / Grad	le 300	θ_{P} θ_{G}
Outside Diameter	D	101.6	mm	
Wall Thickness	t	5.0	mm	
2nd Moment of Area	I	1774693	mm^4	
Yield Strength	Fy	300	N/mm ²	└
Tensile Strength	Ft	400	N/mm ²	

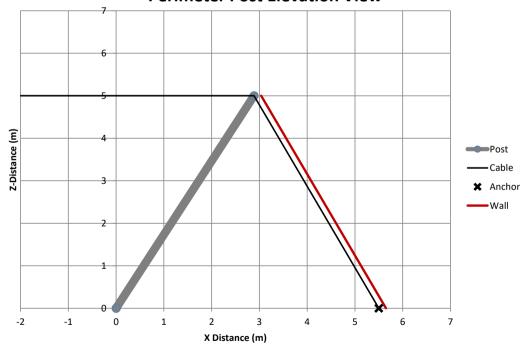
Perimeter Post Configuration

Perimeter Post Location Wall Net Configuration **Anchor Placement Distance** Post Angle

Post Length



Perimeter Post Elevation View



Determination of Guy Loads and Post Compression Loads (using Global Coordinate System)

				Obtained from Anchor worksheet, depends on perimeter
Maximum Cable Load	T_{Cable}	4907	kg	post locations. Based on maximum aerodynamic forces
Maximum Wall Loading	T_{Wall}	1096	kg	Assumes 11/18 of the wall net loading ends up at the top of the post (if applicable)
Total Load at Top of Post	T_Total	6003	kg	Combined Cable & Wall Loading
Guy wire angle	θ_{G}	62.4	deg	Reference to the ground plane.
Maximum Guy load	T_{G_Max}	6158	kg	Note guys evaluated under "Guys" worksheet
Pole Compression	P_{comp}	6302	kg	The maximum load at any part of the column
De l'estate de la contraction				
Bending Moment due to Lateral Deflection				
Maximum lateral deflection after post setting	δy_pp	50.0	mm	ine post must be set straignt on installation. In practise
Equivalent lateral load due this deflection	Py	310	N	this cannot be achieved, so it is assumed that the post top is
Bending moment due this lateral load	M1	1788328	Nmm	displaced the following amount Maximum at base of post, linear distribution.
Secondary moment due compression	M2	3089960	Nmm	Maximum at bottom of post, assuming a square root
,				distribution. Maximum at the centre of the post, assuming a quadratic
Bending moment due wall net loading	М3	0	Nmm	distribution over post height. Only applicable if a wall net is attached to the post.
Stress Calculations				
Axial Stress	fa	49	N/mm²	Based on the post compression found above.
Bending Stress	fb	145	N/mm²	Obtained from the maximum of (M1+M2) at bottom of post or (M3+0.5*M1+0.7071*M2) at middle of post.
<u>Allowables</u>				
Yield Stress	Fy	350	N/mm ²	
Critical Buckling Stress	Fc	133	N/mm ²	
Bending Modulus of Rupture Stress	Fb	430	N/mm ²	
Combined Compression and Bending Interaction	<u>on</u>			
Axial Stress Ratio	Ra	0.37		Bruhn C4.12, use minimum of Fc or Fy
Bending Stress Ratio	Rb	0.34		Bruhn C4.12, use rupture allowable Fb
5				•
Margin of Safety	MS	0.13		Must be greater than zero, includes the factor of safety
Perimeter Post Insert Analysis - Insert is subj	iect to pure	e bending.		
Bending Stress	fb	140	N/mm ²	The bending stress at the bottom of the post
Bending Modulus of Rupture Stress	Fb	400	N/mm²	Assume Ftu for bending failure
Margin of Safety	MS	1.29		Must be greater than zero, includes the factor of safety

Perimeter Post Footing Analysis

Insert Type	Rammed Inser	rt		
Soil description	Loose gravel,	or loose sand an	d gravel	
Soil category		Non-cohesive	soils	_
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter	d	0.53	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.9	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.28	m ²	
Footing shaft area	As	0.32	m ²	Shaft friction
Footing capability	$P_{footing}$	61635	N	
		6285	kg	
Maximum compression load	P_{comp}	6302	kg	
Ratio to Requirement	RtoR	1.00		To remain stable on the ground when subject to the worst combination loading from wind and hail, it is preferable to have this ratio greater than 1.0.

Interior Post

1759-CR01_P&T_Marciano_StructType_27May25

Interior posts are designed to withstand hail loading pulling the net to the ground. The interior posts are staggered in the block and therefore subjected to two bays worth of hail. This analysis assumes that wind loading has displaced the top of the post 100mm (assuming 100% fixed based support), and the post is subject to direct bending due to this displacement and bending due to offset compression.

Select Main Post Material Outside Diameter Outside Diamet	Inputs				
Select Main Post Material Outside Diameter D 114.3 mm Wall Thickness t 3.6 mm Cross Sectional Area A 1252 mm² 2 And Moment of Area I 1919837 mm⁴ Elastic Modulus E 2070000 N/mm² Vield Strength Fy 350 N/mm² Tensile Strength Ft 430 N/mm² Buckling Strength Ft 430 N/mm² Axial Compression due Hail Loading Hail loading associated with each interior post M_hail Saciated with each interior post Area associated with each interior post Post compression Pcomp 18.04 kg Bending Moments due Wind Loading Lateral deflection at top of post due wind Lateral loading associated with this deflection Py 795 N Bending moment due lateral force Mb1 3974062 Nmm Secondary moment due lateral force Mb2 1474422 Nmm Stress Calculations Stress Calculations Three boys for the stoager three metrior post configurations. Three boys for the stoager three metrior post	Description	Variable	Value	Units	Comments
Outside Diameter Outside Diameter Wall Thickness t 3.6 mm Vall Thickness t 3.6 mm 1 1919837 mm ⁴ Elastic Modulus E 207000 N/mm ² Yeled Strength Fy 350 N/mm ² Tensile Strength Ft 430 N/mm ² Buckling Strength Ft 430 N/mm ² Axial Compression due Hail Loading Hail loading associated with each interior post Area associated with each interior post Anet 601 m2 Post compression Post ompression Post of "Loading" worksheet. Post obey for the stoget and two row interior Post ompression Post of "Loading" worksheet. Post obey for the stoget on trained strengt and two row interior Post of "Loading" worksheet. Post obey for the stoget of the "Loading" worksheet		4001	D	250	T
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Post compression Pomp 1804 kg Bending Moments due Wind Loading Lateral deflection at top of post due wind Lateral loading associated with this deflection Py 795 N See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N See the "Loading" worksheet. Name Place Pla					
Post compression Pcomp 1804 kg Bending Moments due Wind Loading Lateral deflection at top of post due wind bending associated with this deflection Py 795 N N See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N N Secondary moment due lateral force Mb1 3974062 Nmm Stress Calculations Stress Calculations Axial Stress fa 14.1 N/mm² Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Use the average of the Yield and Tensile Strength (IP post bending does not failure the structure) Combined Compression and Bending Interaction Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb	Area associated with each internal post	Anet	601	m2	
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Lateral deflection at top of post due wind 8y_ip 83 mm See the "Loading" worksheet. Lateral loading associated with this deflection Py 795 N Seendary moment due lateral force Mb1 3974062 Nmm Secondary moment due lateral deflection Mb2 1474422 Nmm Secondary moment due lateral deflection Mb2 N/mm² Stress Calculations Axial Stress					
Lateral loading associated with this deflection Py 795 N Bending moment due lateral force Mb1 3974062 Nmm Secondary moment due lateral deflection Mb2 1474422 Nmm Stress Calculations Axial Stress fa 14.1 N/mm² Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Bending Moments due Wind Loading				
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Secondary moment due lateral deflection Mb2 1474422 Nmm Stress Calculations Axial Stress fa 14.1 N/mm² Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb		•			
Stress Calculations Axial Stress	_				
Axial Stress fab fa 14.1 N/mm² Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb	Secondary moment due lateral deficetion	IVIDZ	1474422	Nillii	
Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Bending Stress Ratio Ra 0.08 Bending Stress Ratio Rb 0.42 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb	Stress Calculations				
Bending Stress fb 162.2 N/mm² Allowables Yield Stress Fy 350 N/mm² Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Bending Stress Ratio Ra 0.08 Bending Stress Ratio Rb 0.42 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb					
Allowables Yield Stress Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Bending Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb	Axial Stress	fa	14.1	N/mm ²	
Yield Stress Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb	Bending Stress	fb	162.2	N/mm ²	
Yield Stress Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bruhn C4.12, use rupture allowable Fb					
Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Use the average of the Yield and Tensile Strength (IP post bending does not failure the structure) Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Allowables				
Buckling Critical Stress Fc 177 N/mm² Bending Modulus of Rupture Stress Fb 390 N/mm² Use the average of the Yield and Tensile Strength (IP post bending does not failure the structure) Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Viald Strass	Ev	350	N/mm ²	
Bending Modulus of Rupture Stress Fb 390 N/mm² Use the average of the Yield and Tensile Strength (IP post bending does not failure the structure) Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb		•			
Combined Compression and Bending Interaction Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	•				Use the average of the Yield and Tensile Strenath (IP post bending
Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Bending Modulus of Rupture Stress	Fb	390	N/mm²	
Axial Stress Ratio Ra 0.08 Bruhn C4.12, use minimum of Fc or Fy Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb					
Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Combined Compression and Bending Interaction	<u>l</u>			
Bending Stress Ratio Rb 0.42 Bruhn C4.12, use rupture allowable Fb	Axial Stress Ratio	Ra	0.08		Bruhn C4 12 use minimum of Ec or Ev
Margin of Safety MS 0.61 Must be greater than zero, includes the factor of safety	3	-	- · -		, , ,
	Margin of Safety	MS	0.61		Must be greater than zero, includes the factor of safety

Interior Post Footing Analysis

Insert Type	Rammed Insert			
Soil description	Loose gravel, or	loose sand and g	ravel	
Soil category	N	lon-cohesive soi	ls	-
Presumed bearing value	fbr	200	kPa	
Estimated soil shear capability	fs	20	kPa	Estimated as 10% of bearing capacity assuming 100% Settlement Factor
Footing diameter	d	0.29	m	For a concrete footing, "d" is the auger diameter. For a rammed insert, "d" refers to the square dimension (ie metal plate sized "d" x "d").
Footing height	h	0.90	m	Depth of hole or underside length of rammed insert.
Footing bearing area	Ab	0.07	m ²	
Footing shaft area	As	0.32	m^2	Shaft friction
Footing capability	Pfooting	21231 2165	N kg	
Maximum compression load	Dooms			
Maximum compression load	Pcomp	1804	kg	
Ratio to Requirement	RtoR	1.20		Must be greater than 1.0

Guys

1759-CR01_P&T_Marciano_StructType_27May25

All guys are made using a loop of cable from the anchor to the post top. The anchor has a dedicated thimble head that is screwed to the anchor rod, and the post tops have integrated welded thimbles. The cable is threaded through both and butt spliced together to make a loop of cable. The following analyses collates the guy forces worked out in each of the post worksheets, and verifies the strength through a single analysis.

Description	Variable	Value	Units	Comments
Maximum Guy Loads from the Post Analys	es			
Corner Post (55deg)		5542	kg	
Corner Post (TP)		5773	kg	
Corner Post (Angled)		5996	kg	
Corner Post (B2 SE)		6303	kg	Standalone SE Perimeter/Corner Posts
Perimeter Breaker Post (SE)		4325	kg	Breaker post has two guys on A2.
Perimeter Breaker Post		4451	kg	Breaker post has two guys on A2.
Interior Breaker Post		6632	kg	
Perimeter Post (TP)		5780	kg	
Perimeter Post (CG 69deg)		6383	kg	
Perimeter Post (RE)		6158	kg	
				50
Maximum Guy Force	T_{G_Max}	6632	kg	40
Diameter of Thimble	d _{ROPE}	7.5	mm	30 30
Diameter of Thimble		60	mm	E 20
Diameter of Thimble	D _{THIMBLE}	00	111111	erce
Diameter Ratio	D/d	8.0		a. 10
Strength Loss due to Thimble	From Chart	16%		0 10 20 30 40
5. 5. 5. 2000 add to 111111010	Trom chart	1070		D/d ratio FIGURE 17-8 Percent strength loss due to different D/d ratios;
Corrected Guy Breaking Load *		10442	kg	derived from standard test data for 6×19 and 6×17 class ropes.
			J	(From Wire Rope Users Manual, American Iron and Steel Institute [AISI], 1979.)
Margin of Safety	MS	0.26		Must be greater than zero, includes the factor of safety

^{*} Note that G2 Netting Systems regularly tests the guy loops in order to verify cable, splice and thimble strengths. The testing shows strengths greater than 96 kN, which supports the use of the Table 17-8 above.



Anchors

1759-CR01_P&T_Marciano_StructType_27May25

The anchors are sized to withstand the maximum predicted cable load pulling down to the anchor. The maximum cable load is based on wind shear and hail, and is computed on the "Cables" worksheet. The anchor is assumed to be the 250 mm or 350mm equivalent drill anchor using a 24mm steel rod protruding from ground with a screw-on knuckle with thimble (see picture below). The failure modes considered are holding capacity, rod tension and thread shear.

Description	Variable	Value	Units	Comments

Soil Capacity

Soil Classification Soil Description (fit description against site test results) **Anchor Selection** AU350 AU350 Drill Anchor Holding Capacity: 10585 See chart and table below. P_{Anchor} kg

Reference "Chance Anchors Catalogue 4 Dec 2014". Loose to medium dense fine to coarse sands to stiff clays and silts AU350 Jumbo Type Drill Anchor

Anchor Mechanical Capacity

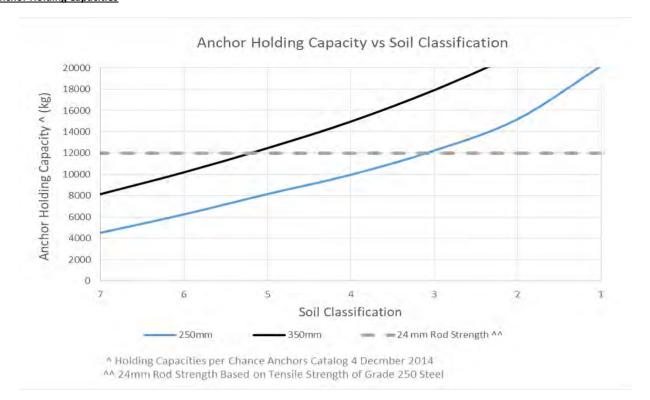
Typical Failure Mode	Nut thread strips out or tension failure of rod						
Thread Type		M24 x 2.5					
Rod Diameter away from threaded ends	d_0	22	mm				
Thread Nominal Diameter	d_p	24	mm				
Thread Pitch	р	2.5	mm				
Minor Diameter	d1	20.9	mm				
Pitch Diameter	d2	22.4	mm				
Tensile Stress Area (threaded section)		368	mm^2	Shigley p 293 1st metric edition, avg of d1 and d2.			
Tensile Stress Area (away from threaded ends)		380	mm^2				
Nut height	h	25	mm	Assume using the Jumbo Anchors with knuckle.			
Yield Strength	Fty	300	N/mm2				
Shear Strength	Fsu	173	MPa				
Nut Thread Shear Allowable	P_thread	15510	kg	Based on the minimum thread engagement at either end.			
Rod Tension Allowable	P_tension	11267	kg	Based on the yield allowable.			
Minimum Anchor Allowable Load	P _{Anchor_Allow}	10585	kg	Minimum of P_anchor, P_thread, and P_tension			
Maximum Anchor Pull Load	P _{Anchor_Max}	6632	kg	Equates to the maximum guy force in worksheet "Guys"			
Margin of Safety (Guy load to anchor allowable)	MS	0.28		Must be greater than zero, includes the factor of safety			

Notes: 1) During installation the anchor may be upgraded to the 350 mm size if the installation torque is below specification. 2) If any anchor moves in the ground, it is not regarded as a failure. Anchor movement results in the slackening of the structure locally, with cable, post and guy loads reducing. If over time the anchor continues to move, additional anchorage is then employed.





Anchor Holding Capacities



Class	Common Soil-Type Description	Geological Soil Classification
0	Sound hard rock, unweathered (bedrock)	Granite, Basalt, Massive Limestone
1	Very dense and/or cemented sands; coarse gravel and cobbles	Caliche, (Nitrate-bearing gravel/rock),
2	Dense fine sands; very hard silts and clays (may be preloaded)	Basal till; boulder clay; caliche; weathered laminated rock
3	Dense sands and gravel; hard silts and clays	Glacial till; weathered shales, schist, gneiss and siltstone
4	Medium dense sand and gravel; very stiff to hard silts and clays	Glacial till; hardpan; marls
5	Medium dense coarse sands and sandy gravels; stiff to very stiff silts and clays	Saprolites, residual soils
6	Loose to medium dense fine to coarse sands to stiff clays and silts	Dense hydraulic fill; compacted fill; residual soils
**7	Loose fine sands; Alluvium; loess; medium - stiff and varied clays; fill	Flood plain soils; lake clays; adobe; gumbo, fill
**8	Peat, organic silts; inundated silts, fly ash very loose sands, very soft to soft clays	Miscellaneous fill, swamp marsh

^{***} Anchors are required to be drilled deeper, by use of extensions, to penetrate Class 5 or 6 underlying the Class 7 and 8 soils.



Appendix CCertificate of Title







Provided by CITEC Confirm

NEW SOUTH WALES LAND REGISTRY SERVICES - TITLE SEARCH

FOLIO: 2/1248259

SEARCH DATE	TIME	EDITION NO	DATE	
25/6/2025	12:04 PM	3	13/5/2021	

LAND

LOT 2 IN DEPOSITED PLAN 1248259

AT MONAK

LOCAL GOVERNMENT AREA WENTWORTH
PARISH OF PARINGI COUNTY OF WENTWORTH
TITLE DIAGRAM DP1248259

FIRST SCHEDULE

P & E MARCIANO PTY LTD

(T AP86594)

SECOND SCHEDULE (12 NOTIFICATIONS)

- 1 RESERVATIONS AND CONDITIONS IN THE CROWN GRANT(S) WITHIN THE PART(S) SHOWN SO INDICATED IN THE TITLE DIAGRAM
- 2 I155249 LAND EXCLUDES MINERALS WITHIN THE PART(S) SHOWN SO INDICATED IN THE TITLE DIAGRAM
- 3 DP827371 RIGHT OF CARRIAGEWAY 4 METRE(S) WIDE AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 4 DP827371 RIGHT OF CARRIAGEWAY 4 METRE(S) WIDE APPURTENANT TO THE LAND ABOVE DESCRIBED
- 5 DP827371 RIGHT OF CARRIAGEWAY 6 METRE(S) WIDE AND VARIABLE WIDTH AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 6 DP827371 RIGHT OF CARRIAGEWAY 6 METRE(S) WIDE AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 7 DP827371 EASEMENT FOR PIPELINE 6 METRE(S) WIDE AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 8 DP827371 EASEMENT FOR PIPELINE 3 METRE(S) WIDE AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM
 - DP1248259 EASEMENT RELEASED IN SO FAR AS IT BENEFITS LOT 6
 IN DP827371
- 9 DP827371 EASEMENT FOR PIPELINE 3 METRE(S) WIDE APPURTENANT TO THE LAND ABOVE DESCRIBED
 - DP1248259 EASEMENT RELEASED IN SO FAR AS IT AFFECTS LOT 6
 IN DP827371
- 10 DP827371 EASEMENT FOR PIPELINE 6 METRE(S) WIDE AND VARIABLE

AFFECTING THE PART(S) SHOWN SO BURDENED IN THE TITLE

DIAGRAM

11 DP827371 EASEMENT FOR PUMP SITE 9.40 METRE(S) WIDE AFFECTING

THE PART(S) SHOWN SO BURDENED IN THE TITLE DIAGRAM

12 AR45254 MORTGAGE TO AUSTRALIA AND NEW ZEALAND BANKING GROUP

END OF PAGE 1 - CONTINUED OVER

20071 PRINTED ON 25/6/2025

NEW SOUTH WALES LAND REGISTRY SERVICES - TITLE SEARCH

FOLIO: 2/1248259 PAGE 2

SECOND SCHEDULE (12 NOTIFICATIONS) (CONTINUED)

LIMITED

NOTATIONS

UNREGISTERED DEALINGS: NIL

*** END OF SEARCH ***

Page 2 of 3

20071

PRINTED ON 25/6/2025

Provided on 25/06/2025 12:04 PM by CITEC Confirm

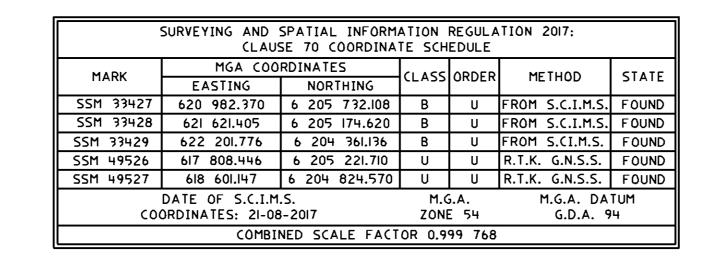
* Any entries preceded by an asterisk do not appear on the current edition of the Certificate of Title. Warning: the information appearing under notations has not been formally recorded in the Register.

CITEC Confirm hereby certifies that the information contained in this document has been provided electronically by the Registrar General in accordance with section 96B(2) of the Real Property Act, 1900.

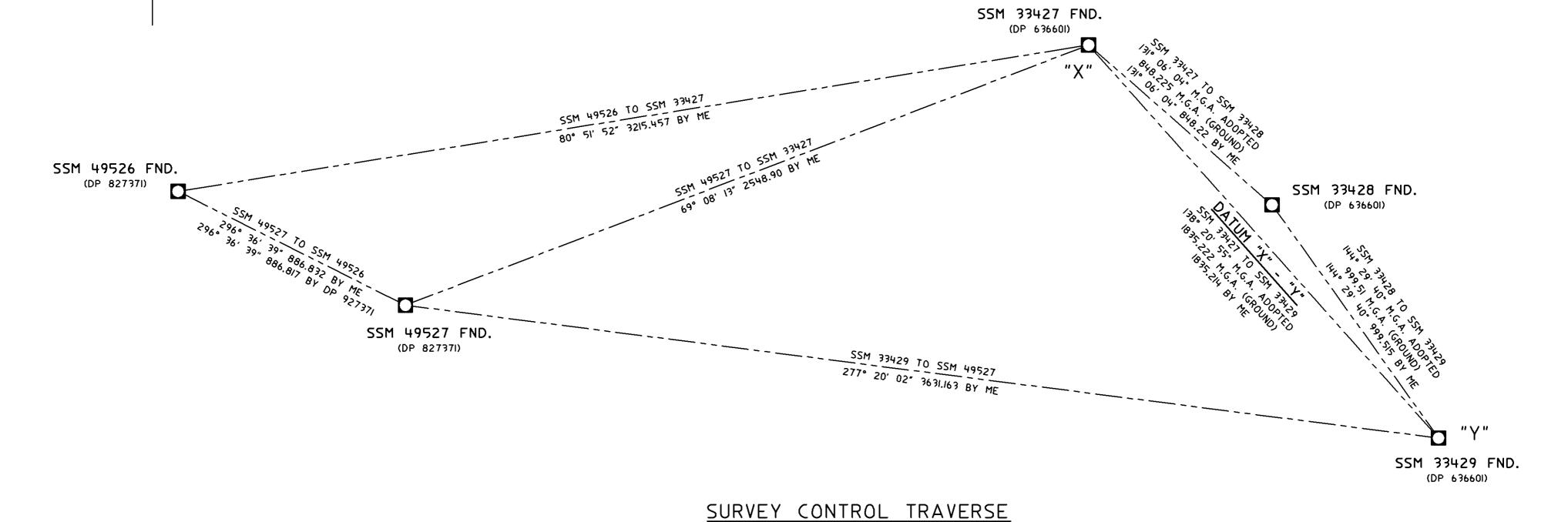
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Page 3 of 3



	G.N.S.S. VAL	IDATION SCHED	ULE	
FROM	TO	GRID BEARING	DISTANCE	METHOD
SSM	SSM	138° 20′ 55″	1835.214	R.T.K. G.N.S.S.
33427	323429	138° 20′ 55″	1835.222	S.C.I.M.S.



NOTES:-

G.N.S.S. OBSERVATIONS WERE USED TO DRIVE DIMENSIONS OF THE SURVEY CONTROL TRAVERSE, CONNECTIONS AND THE DISTANCES OF THE BOUNDARIES OF THE SITE THAT ARE GREATER THAN 100 METRES

PETER ROBERT DANSON

PLAN OF SUBDIVISION OF LOTS 3 AND 6 IN DP 827371 LGA: WENTWORTH PARINGI MONAK Locality:

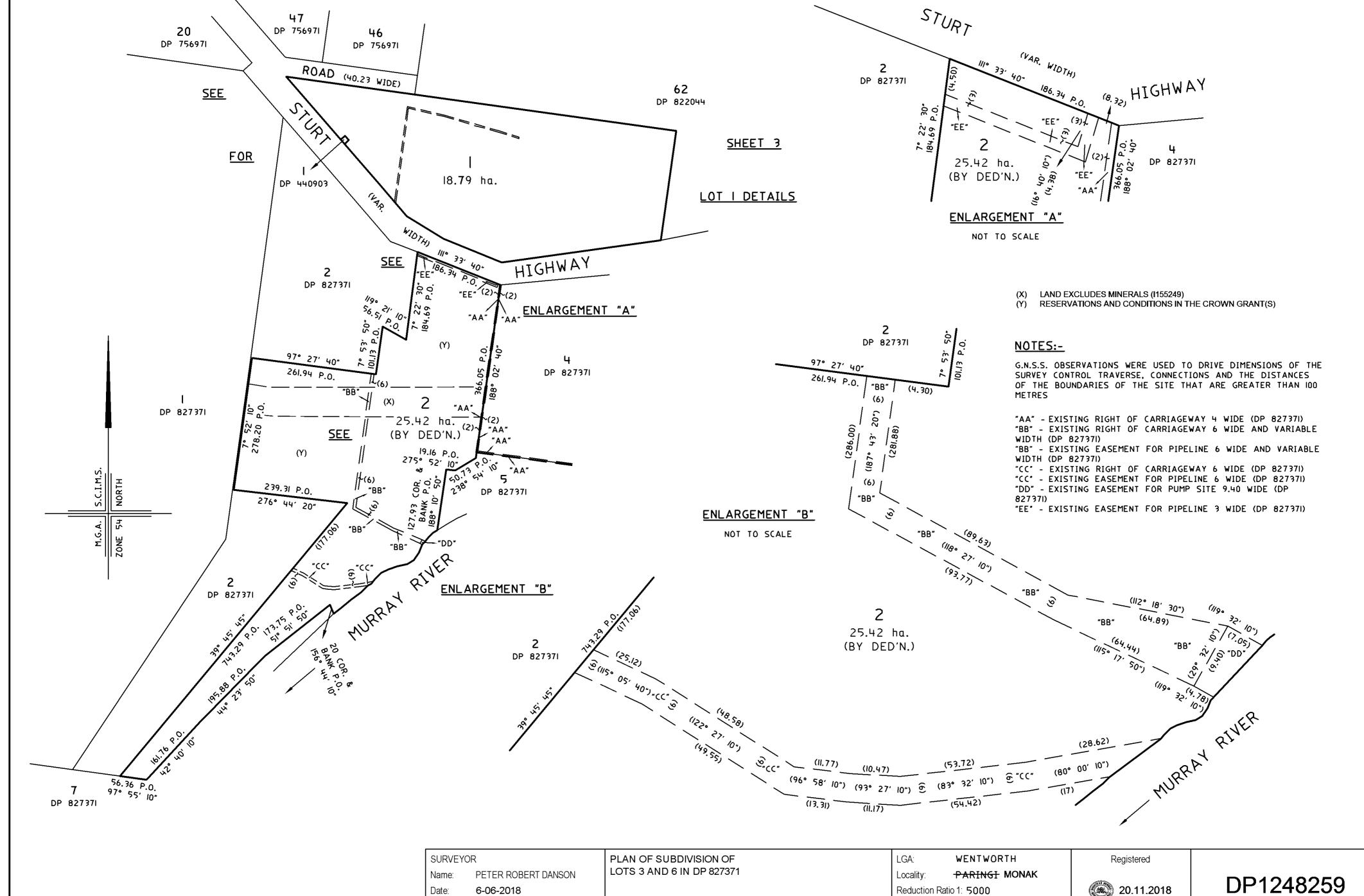
Reduction Ratio 1: 10000 Lengths are in metres.

Registered

DP1248259

AMENDED IN NSW LRS AT THE SURVEYOR'S REQUEST 20.11.2018

/Seq:2



Reference: 9281

Reduction Ratio 1: 5000

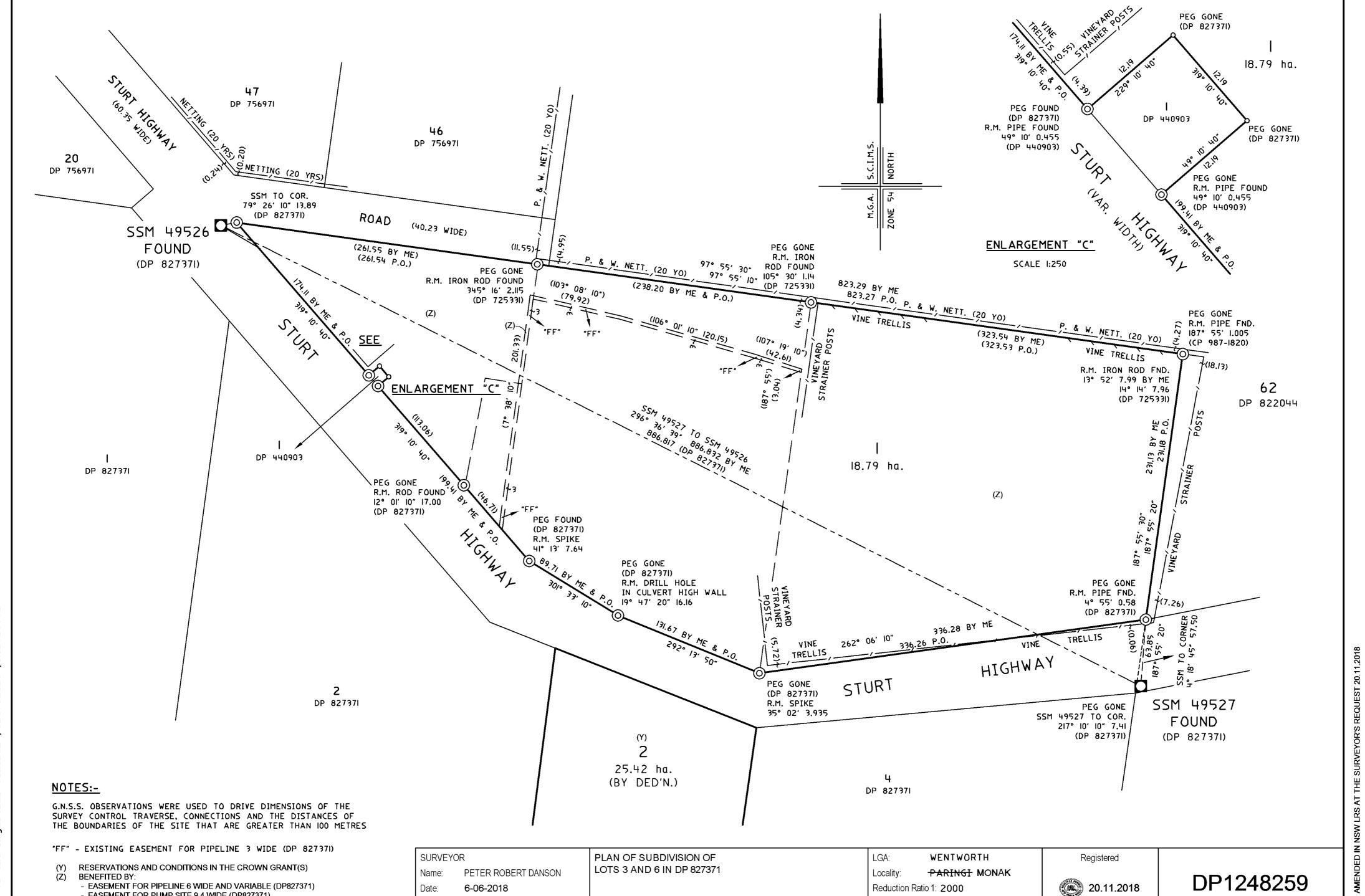
Lengths are in metres.

20.11.2018

DP1248259

UEST 20.11.2018

AMENDED IN NSW LRS AT THE SURVEYOR'S REQI



Reduction Ratio 1: 2000

Lengths are in metres.

6-06-2018

Date:

Reference: 9281

ov-2018 /NSW LRS CITEC /Ref:20071 /Doc:DP 1248259 P /Rev:20-N the Registrar-General /Src: Req:R482669 © Office of

- EASEMENT FOR PIPELINE 6 WIDE AND VARIABLE (DP827371)

- EASEMENT FOR PUMP SITE 9.4 WIDE (DP827371)

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PLAN FORM 6 (2017) DEPOSITED PLAN PLAN ADMINISTRATION SHEET Sheet 1 of & Sheet(s) Office use only se only 20.11.2018 Registered: DP1248259 S Title System: TORRENS PLAN OF SUBDIVISION OF LGA: **WENTWORTH** LOTS 3 AND 6 IN DP 827371 Locality: MONAK Parish: **PARINGI** County: **WENTWORTH** Survey Certificate Crown lands NSW/Western Lands Office Approval PETER ROBERT DANSON (Authorised Officer) in approving this plan certify that all necessary approvals in regard to the of 177 WALNUT AVENUE MILDURA allocation of the land shown herein have been given. a surveyor registered under the Surveying and Spatial Information Act 2002, certify that: Signature: *(a) The land shown in the plan was surveyed in accordance with the Date: Surveying and Spatial Information Regulation 2017, is accurate File Number: and the survey was completed on, or *(b) The part of the land shown on the plan (*being/*excluding**......... LOT L AND CONNECTIONS was surveyed in accordance with the Surveying and Spatial Information Regulation 2017, the part surveyed is accurate and Subdivision Certificate the survey was completed on 6-06-2018 the part not KEN ROSS surveyed was compiled in accordance with that Regulation, or *Authorised Person/*Ceneral Manager/*Accredited Certifier, certify that the provisions of the s. 109J of the Environmental Planning and *(c) The land shown in this plan was compiled in accordance with the Assessment Act 1979 have been satisfied in relation to the proposed Surveying and Spatial Information Regulation 2017. subdivision, new road or reserve set out herein. Datum Line "X" - "Y" Signature: Type"*Urban/*Rural Accreditation number: The terrain is "Level-Undulating/*Steep Mountainous... Date of endorsement: 1 AUGUST 2018 Subdivision Certificate number: 09/18 File Number: DA2017|1391 Surveyor Identification No: 902 Surveyor registered under the Surveying and Spatial Information Act 2002 *Strike through if inapplicable *Strike out inappropriate words. **Specify the land actually surveyed or specify any land shown in the plan that is not the subject of the survey. Plans used in the preparation of survey/compilation. Statements of intention to dedicate public roads, create public reserves and drainage reserves, acquire/resume land. CP 987-1820 CP 988-1820 DP 440903 DP 63660I DP 725331 DP 827371 Signatures, Seals and Section 88B Statements should appear on Surveyor's Reference: 9281 PLAN FORM 6A

Req:R482669 /Doc:DP 1248259 P /Rev:20-Nov-2018 /NSW LRS /Pgs:ALL /Prt:25-Jun-2025 15:35 /Seq:5 of 7 © Office of the Registrar-General /Src:CITEC /Ref:20071

PLAN FORM 6A (2017) DEPOSITED PLAN PLAN ADMINISTRATION SHEET Sheet 2 of 2 Sheet(s) Office use only 20.11.2018 Registered: DP1248259 PLAN OF SUBDIVISION OF LOTS 3 AND 6 IN DP 827371 This sheet is for the provision of the following information as required: A Schedule of lots and addresses - See 60(c) SSI Regulation 2017 Statements of intention to create and release affecting interests in 09/18 Subdivision Certificate number: accordance with section 88B Conveyancing Act 1919. 01.08.2018 Date of endorsement: Signatures and seals - see 195D Conveyancing Act 1919. Any information which cannot fit in the appropriate panel of sheet 1 of the administration sheets.

STREET ADDRESSES OF ALL LOTS ARE NOT AVAILABLE

PURSUANT TO SECTION 88B OF THE CONVEYANCING ACT 1919, AS AMENDED, IT IS INTENDED TO RELEASE:

- EASEMENT FOR PIPELINE 3 WIDE (DP 82737I)
- EASEMENT FOR PIPELINE 3 WIDE (DP 82737I)

If space is insufficient use additional annexure sheet.

Surveyor's Reference: 9:

9281

PLAN FORM 6A (2017) DEPOSITED PLAN ADMINISTRATION SHEET Sheet 3 of 4 sheet(s)				
Registered: 20.11.2018 PLAN OF SUBDIVISION OF LOTS 3 AND 6 IN DP 827371	DP1248259 This sheet is for the provision of the following information as required: • A schedule of lots and addresses - See 60(c) SSI Regulation 2017			
Subdivision Certificate number: 09/18 Date of Endorsement: 1 August 2018	 Statements of intention to create and release affecting interests in accordance with section 88B Conveyancing Act 1919 Signatures and seals- see 195D Conveyancing Act 1919 Any information which cannot fit in the appropriate panel of sheet 1 of the administration sheets. 			
Executed by Karambi Producers Pty Ltd ACN 075 708 324 in accordance with Section 127 of the Corporations Act 2001 by being signed by those persons who are Authorized to sign the company Director Print Name Print name GARRY Cox SHORE				
Executed by P & E Marciano Pty Ltd ACN 075 708 324 in accordance with Section 127 of the Corporations Act 2001 by being signed by those persons who are Authorized to sign the company Sole Director/Secretary Print Name X FILIPPO MARCIANO				
If space is insufficient us Surveyor's Reference: 9281	se additional annexure sheet			

Witness Signature
HUGH FLETT
GRIBUSINESS MANAGER

witness Name

55 DEAKIN AVENUE MILDURA VIC 3500

Wilmess Address.

If space is insufficient use additional annexure sheet

Surveyor's Reference: 9281

INSTRUMENT SETTING OUT TERMS OF EASEMENTS AND RESTRICTION AS TO USER INTENDED TO BE CREATED PURSUANT TO SECTION 88B CONVEYANCING ACT 1919



DP1248259 B

Full name and address of owner of Lot 3 in DP 827371

Full name and address of owner of Lot 6 in DP 827371

(Sheet 1 of 3 Sheets)

PLAN OF SUBDIVISON OF LOTS 3 AND 6 IN DP 827371 SUBDIVISION CERTIFICATE NO.: 09/18

Karambi Producers Pty Limited (ACN 075 708 324) 5750 Sturt Highway, Monak 2738

P & E Marciano Pty Ltd (ACN 119608874) 327 Morpung Avenue, Irymple 3498

PART 1A (Release)

Number of item	Identity of easement,	Burdened	Benefited lot(s),
shown in the	profit a` prendre, to be	lot(s) or	road(s), bodies or
intention panel on	released and referred to	parcel(s):	Prescribed
the plan	in the plan		Authorities:
1	Easement for pipeline 3	3/827371	6/827371
	wide (DP827371)		
2	Easement for pipeline 3	6/827371	3/827371
	wide (DP827371)		

INSTRUMENT SETTING OUT TERMS OF EASEMENTS AND RESTRICTION AS TO USER INTENDED TO BE CREATED PURSUANT TO SECTION 88B CONVEYANCING ACT 1919

(Sheet 2 of 3 Sheets)

DP1248259

X FILIPPO MARCIANO PLAN OF SUBDIVISON OF LOTS 3 AND 6 IN DP 827371 SUBDIVISION CERTIFICATE NO.: 09/18

Executed by Karambi Producers Pty Ltd)
ACN 075 708 324 in accordance with)
Section 127 of the Corporations Act 2001)
by being signed by those persons who are)
Authorized to sign the company)
Cam 4	Slose
Director	Director/Secretary
Print Name	Print name
GARRY COX	Print name GMARON COX
	·
Executed by P & E Marciano Pty Ltd)
ACN 075 708 324 in accordance with)
Section 127 of the Corporations Act 2001)
by being signed by those persons who are)
Authorized to sign the company)
P. Man	
Sole Director/Secretary	
Print Name	

INSTRUMENT SETTING OUT TERMS OF EASEMENTS AND RESTRICTION AS TO USER INTENDED TO BE CREATED PURSUANT TO SECTION 88B CONVEYANCING ACT 1919

(Sheet 3 of 3 Sheets)

DP1248259

PLAN OF SUBDIVISON OF LOTS 3 AND 6 IN DP 827371 SUBDIVISION CERTIFICATE NO.: 09/18

NATIONAL AUSTRALIA BANK consent in relation to Mortgage 3831930

Executed on behalf of the National Australia Bank
Limited by its Attorney
who holds the position of Level 3 Attorney under Power
of Attorney dated 1 March 2007 on the presence of:

Sarah Clothier Name of Witness

Signature of Attorney

Mortgagee under Mortgage NO. 3831930
Signed at Mildura whis 16th day of August 2018
for National Australia Bank Limited ABN 12004044937
by Advian Paul Hardie its duly appointed Attorney
under Power of Attorney No. 39 Book 4512

Attorney gignature, Level 3 Attorney.

widness Signature.

HUGH FLETT AGRIBUSINESS MANAGER

witness Name.

55 DEAKIN AVENUE MILDURA VIC 3500

witness Address.







Provided by CITEC Confirm

NEW SOUTH WALES LAND REGISTRY SERVICES - TITLE SEARCH

FOLIO: 2/827371

SEARCH DATE	TIME	EDITION NO	DATE
22/8/2025	12:06 PM	8	13/5/2021

TIAND

LOT 2 IN DEPOSITED PLAN 827371

AT MONAK

LOCAL GOVERNMENT AREA WENTWORTH
PARISH OF PARINGI COUNTY OF WENTWORTH
TITLE DIAGRAM DP827371

FIRST SCHEDULE

P & E MARCIANO PTY LTD

(T AM209341)

SECOND SCHEDULE (11 NOTIFICATIONS)

- 1 RESERVATIONS AND CONDITIONS IN THE CROWN GRANT(S)
- 2 DP827371 RIGHT OF CARRIAGEWAY 4 WIDE AFFECTING THE PART OF THE LAND ABOVE DESCRIBED SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 3 DP827371 RIGHT OF CARRIAGEWAY 6 WIDE AFFECTING THE PART OF THE LAND ABOVE DESCRIBED SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 4 DP827371 EASEMENT FOR PIPELINE 6 WIDE AFFECTING THE PART OF THE LAND ABOVE DESCRIBED SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 5 DP827371 EASEMENT FOR PIPELINE 3 WIDE AFFECTING THE PART OF THE LAND ABOVE DESCRIBED SHOWN SO BURDENED IN THE TITLE DIAGRAM
- 6 DP827371 RIGHT OF CARRIAGEWAY APPURTENANT TO THE LAND ABOVE DESCRIBED
- 7 DP827371 RIGHT OF CARRIAGEWAY 6 WIDE AND VARIABLE APPURTENANT TO THE LAND ABOVE DESCRIBED
- 8 DP827371 EASEMENT FOR PIPELINE 3 WIDE APPURTENANT TO THE LAND ABOVE DESCRIBED
- 9 DP827371 EASEMENT FOR PIPELINE 6 WIDE AND VARIABLE APPURTENANT TO THE LAND ABOVE DESCRIBED
- 10 DP827371 EASEMENT FOR PUMP SITE 9.40 WIDE APPURTENANT TO THE LAND ABOVE DESCRIBED
- 11 AR45254 MORTGAGE TO AUSTRALIA AND NEW ZEALAND BANKING GROUP

LIMITED

NOTATIONS

END OF PAGE 1 - CONTINUED OVER

20071 PRINTED ON 22/8/2025

NEW SOUTH WALES LAND REGISTRY SERVICES - TITLE SEARCH

FOLIO: 2/827371 PAGE 2

NOTATIONS (CONTINUED)

UNREGISTERED DEALINGS: NIL

*** END OF SEARCH ***

20071

PRINTED ON 22/8/2025

Provided on 22/08/2025 12:06 PM by CITEC Confirm

* Any entries preceded by an asterisk do not appear on the current edition of the Certificate of Title. Warning: the information appearing under notations has not been formally recorded in the Register.

CITEC Confirm hereby certifies that the information contained in this document has been provided electronically by the Registrar General in accordance with section 96B(2) of the Real Property Act, 1900.

Information contained in this document is provided by CITEC Confirm, ABN 52 566 829 700, confirm.com.au, an approved NSW Land Registry Services Information Broker.

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Page 3 of 3



Appendix D

Dial Before You Dig Service Maps



Redlands 5721b Sturt Hwy



Review responses online >



Received 3 of 3 responses All responses received

Redlands 5721b Sturt Hwy, Monak NSW 2738

Job dates 31/10/2025 → 31/12/2025

These plans expire on 23 Jul 2025

Lodged by Jasmine Walters

Status	Page
	2
Received	4
Received	13
Received	19
	Received Received

Zero damage - Zero harm - Zero disruption

Contact Details

 Contact
 Contact number
 Company
 Enquirer ID

 Jasmine Walters
 (08) 8193 5600
 MasterPlan Pty Ltd
 3600898

Email

jasminew@masterplan.com.au

Address
338a Carrington Street

Adelaide SA 5000

Job Site and Enquiry Details

WARNING: The map below only displays the location of the proposed job site and does not display any asset owners' pipe or cables. The area highlighted has been used only to identify the participating asset owners, who will send information to you directly.

Enquiry date	Start date	End date	On behalf of	Job purpose	Locations	Onsite activities
25/06/2025	31/10/2025	31/12/2025	Private	Design	Private	Planning & Design



Check that the location of the job site is correct. If not, you must submit a new enquiry.

If the scope of works change or plan validity dates expire, you must submit a new enquiry.

Do NOT dig without plans. Safe excavation is your responsibility. If you don't understand the plans or how to proceed safely, please contact the relevant asset owners.

User Reference Redlands 5721b Sturt Hwy Address Redlands 5721b Sturt Hwy Monak NSW 2738 Notes/description

_

Your Responsibility and Duty of Care

- Lodging an enquiry does not authorise project commencement. Before starting work, you must obtain all necessary information from all affected asset owners.
- If you don't receive plans within 2 business days, contact the asset owner & quote their sequence number.
- Always follow the 5Ps of Safe Excavation (page 2), and locate assets before commencing work.
- Ensure you comply with State legislative requirements for Duty of Care and safe digging.
- If you damage an underground asset, you MUST advise the asset owner immediately.
- By using the BYDA service, you agree to the Privacy Policy and Term of Use.
- For more information on safe digging practices, visit www.byda.com.au

Asset Owner Details

Below is a list of asset owners with underground infrastructure in and around your job site. It is your responsibility to identify the presence of these assets. Plans issued by Members are indicative only unless specified otherwise. Note: not all asset owners are registered with BYDA. You must contact asset owners not listed here directly.

Referral ID (Seq. no)	Authority Name	Phone	Status
257040418	Essential Energy	13 23 91	NOTIFIED
257040419	Powercor - Mildura	13 22 06	NOTIFIED
257040420	Telstra VICTAS	1800 653 935	NOTIFIED

END OF UTILITIES LIST



Plan

Plan your job. Use the BYDA service at least one day before your job is due to begin, and ensure you have the correct plans and information required to carry out a safe project.



Prepare

Prepare by communicating with asset owners if you need assistance. Look for clues onsite. Engage a skilled Locator.



Pothole

Potholing is physically sighting the asset by hand digging or hydro vacuum extraction.



Protect

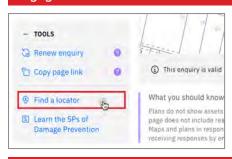
Protecting and supporting the exposed infrastructure is the responsibility of the excavator. Always erect safety barriers in areas of risk and enforce exclusion zones.



Proceed

Only proceed with your excavation work after planning, preparing, potholing (unless prohibited), and having protective measures in place.

Engage a skilled Locator



When you lodge an enquiry you will see skilled Locators to contact

Visit the Certified Locator website directly and search for a locator near you

certloc.com.au/locators

Get FREE Quotes for Contractors & Equipment Fast



Use iseekplant's FREE marketplace to get quotes for the equipment or services you need on your project. Compare quotes from trusted local contractors and get your project done on time and in budget.

- 1. Fill out your job details in our FREE quick quote form.
- 2. We send the request to trusted local contractors.
- 3. The local contractors will contact you directly with quotes

GET QUOTE

Use iseekplant to find trusted contractors near you today, visit: blog.iseekplant.com.au/byda-isp-get-quotes

Book a FREE BYDA Session



BYDA offers free training sessions to suit you and your organisation's needs covering safe work practices when working near essential infrastructure assets. The free sessions are offered in two different formats online and face-to-face.

To book a session, visit:

byda.com.au/contact/education-awareness-enquiry-form

BOOK NOW

Essential Energy

Referral Member Phone 257040418 13 23 91

Responses from this member

Response received Wed 25 Jun 2025 3.53pm

File name	Page
Response Body	5
EW_ASSETS_FOUNDsafetyNotice.pdf	6
plot16106385239213752223.pdf	10
Coversheet_EW_ASSETS_FOUND.pdf	11

Asset Name: 50215

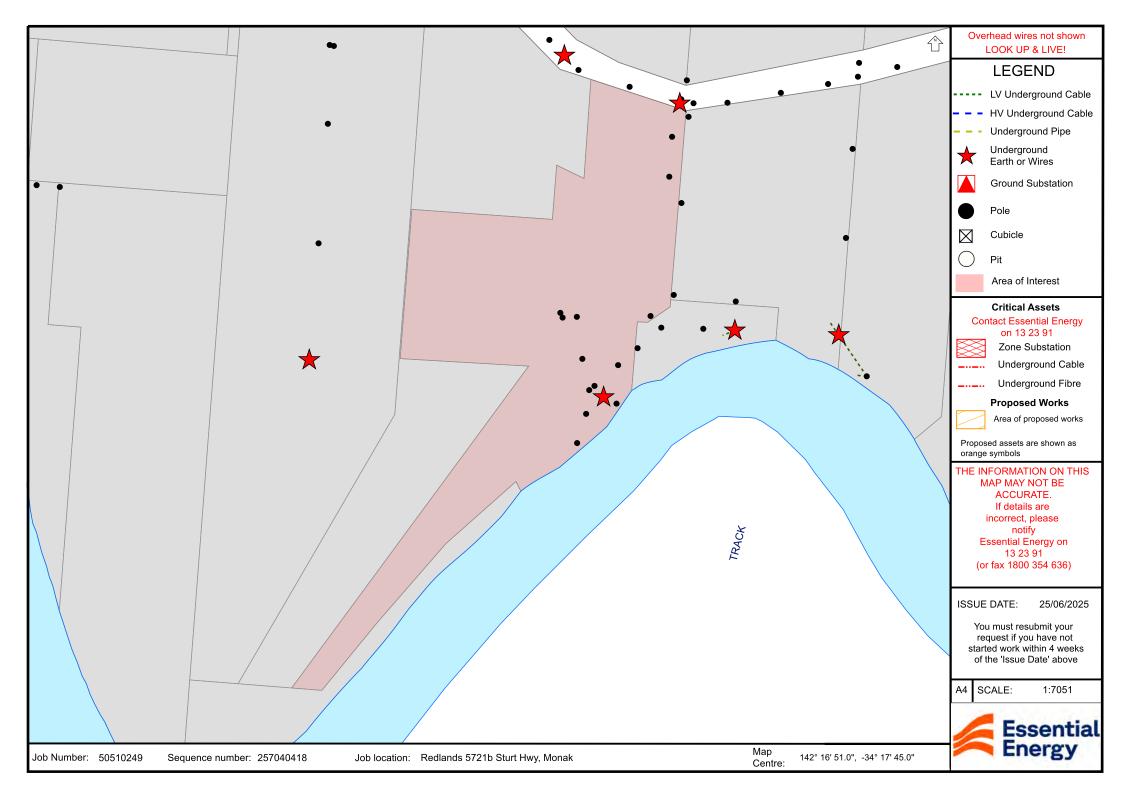
Date of enquiry: 25/06/2025 4:21:00 PM Notification No: 50510249 (Job No)

Sequence No: 257040418

Customer's Name: Jasmine Walters Customer's Phone No: +61881935600

Address supplied for dig site location Redlands 5721b Sturt Hwy, Monak, NSW

You will require a PDF viewer such as Adobe Acrobat Reader to view the attached documents. Adobe Acrobat Reader is freely available at http://get.adobe.com/reader/.





CABLE/PIPE LOCATION

Assets were found in the search area

COMPANY NAME:	MasterPlan Pty Ltd
ATTENTION:	Jasmine Walters
SEARCH LOCATION:	Redlands 5721b Sturt Hwy Monak NSW 2738
SEQUENCE NO:	257040418
DATE:	Wednesday, 25 June 2025

Provision of Plans:

Please find enclosed plans depicting approximate locations of **Essential Energy** assets in the search location. The excavator must not assume that there may not be assets owned by <u>other</u> network operators in the search location.

Underground assets searched for	Underground assets found	
Essential Energy Electrical	Y	
Essential Energy Water & Sewerage		

Plans are updated from time to time to record changes to underground assets and may be updated by Essential Energy without notice. In the event that excavation does not commence within 28 days of receipt of a plan, a new plan should be obtained.

The excavator must retain the plans on site for the duration of the works.

The excavator shall report all damage made to Essential Energy assets immediately. Note that damage includes gouges, dents, holes and gas escapes.

IN CASE OF EMERGENCY OR TO REPORT DAMAGE:	
PHONE 13 20 80	

DISCLAIMER

Please be aware that plans may **not** reflect alterations to surface levels or the position of roads, buildings, fences etc. **Cable and pipe locations are approximate**, and the plans are **not** suitable for scaling purposes. *Essential Energy does not retain plans for privately-owned underground electrical or water* & sewerage assets located on private property. <u>Privately-owned underground electrical assets located on private property are the responsibility of the owner.</u>

The plans have been prepared for Essential Energy's sole use and benefit. **Essential Energy cannot and does not warrant the accuracy or completeness of the plans**. Essential Energy supplies them at no cost with the object of reducing the serious risk of unintentional damage being caused to its cables and pipes. **Essential Energy does not accept any responsibility for any omissions, inaccuracies or errors in the plans, or any reliance place on the material. Any reliance placed on any plan provided in response to your request is at your own risk.**



Essential Energy retains all intellectual and industrial property rights which exists or may exist in or with respect to the plan(s). The material provided is not to be copies or distributed beyond you.

You release Essential Energy from and against all claims, demands, actions and proceedings arising out of or in any way related to the use of the provided material.

Location of Assets on Site:

The plans indicate only that cables and pipes may exist in the general vicinity – they do not pinpoint the exact location of the cables and pipes.

If it is found that the location of cables or pipes on the plans can be improved, please notify Essential Energy on 13 23 91.

All individuals have a duty of care they must observe when working in the vicinity of underground cables and pipes. It is the **excavator's responsibility to visually expose the underground cables and pipes manually**, **ie. by using hand-held tools and non-destructive pot-holing techniques prior to any mechanical excavation.** The excavator will be held responsible for all damage caused to the Essential Energy network or cables and pipes, and for the costs associated with the repair of any such damage. The excavator will also be held responsible for all damage caused to any persons.

When digging in the vicinity of underground assets, persons should observe the requirements of the applicable Codes of Practice published by the NSW Work Cover Authority or Safe Work Australia, and any amendments from time to time by the Authorities, including although not limited to:

- Excavation Work
- Managing Electrical Risks in the workplace
- How to manage and control asbestos in the workplace

(Please refer to https://www.nsw.gov.au/search?q=codes+of+practice)

When digging in the vicinity of **electrical assets** persons should observe the requirements of the **Electricity Supply Act 1995.**

Persons excavating near live underground electrical reticulation and/or earthing cables **must exercise extreme** caution at all times and adhere to the requirements of Essential Energy's Electrical Safety Rules. (These are available on our website: http://www.essentialenergy.com.au/content/safety-community and include:

- Company Procedure: Work Near Essential Energy's Underground Assets
- Asbestos Fact Sheet

In some situations, these procedures call for work to be performed by authorised staff. Should there be any doubt as to the exact location of any underground electrical assets, and the potential for conflict with live underground cables caused by excavation at your work site, you should contact 13 23 91 to arrange for an on-site visit by an Essential Energy representative. No construction or mechanical excavation work is to commence prior to this on-site visit and approval being obtained.

When digging in the vicinity of water or sewer assets persons should observe the requirements of the Water Management Act 2000.

Should there be any doubt as to the exact location of any underground water and sewer assets, and the potential for conflict with underground water and sewer pipes caused by excavation at your work site, you should contact 13 23 91 to arrange for an on-site visit. No construction or excavation work is to commence prior to this on-site visit and approval being obtained.

Prior Notification:

Please note that for excavation depths greater than 250mm near power poles and stays you should allow for **advance notice** in your construction program to permit Essential Energy time to allocate the necessary field resources to carry out the inspection at the site a **minimum of fourteen (14) working days prior to work commencing.**

For further information please call 13 23 91.

Referral 257040419

Member Phone 13 22 06

Responses from this member

Response received Wed 25 Jun 2025 7.27pm

File name	Page
Response Body	14
CitiPower Powercor UG Electricity Hazard Awareness Instructions.pdf	15
257040419 - Citipower Powercor Response letter.pdf	17
257040419 - Citipower Powercor Overview Plan.pdf	18

This referral has been successfully processed by CitiPower Ltd / Powercor Australia Ltd and the results are contained in the attached files.

Understanding your DBYD Response Files

- Read the "257040419 Citipower Powercor Response letter.pdf" and the "CitiPower Powercor UG Electricity Hazard Awareness Instructions.pdf" documents for an overview of your impact on CitiPower/Powercor assets and your obligations
- The remaining (PDF) attachments are detailed construction drawings within your area of works.
- Attachments over 13MB are split into multiple emails (eg, Part 1 of X) ensure you have all documents

Please DO NOT REPLY TO THIS EMAIL as it has been automatically generated and replies are not monitored.

Sequence No: 257040419 Date: 25 Jun 2025

Enquirer: MasterPlan Pty Ltd Contact: Jasmine Walters

Email: qe2vck1mnp9877.drsmm5nta8n1jj@smarterwx-mail.byda.com.au

Phone: +61881935600

Address: 338a Carrington Street, Adelaide SA Site Address: Redlands 5721b Sturt Hwy, Monak NSW

Activity: Planning & Design

Job Number: 50510249

If you require assistance, clarification or Permit to Works please contact 132 206.

We thank you for your enquiry and appreciate your continued use of the "Dial Before You Dig" service.

UNDERGROUND ELECTRICITY HAZARD AWARENESS INSTRUCTIONS





For CitiPower & Powercor Dial Before You Dig customers

Always complete a Dial Before You Dig request before you proceed with any work plans



If there are Underground Electricity assets identified within your work area please ensure that you carefully evaluate all of the information provided

If any part of your proposed works impacts on the **EXCLUSION ZONES** shown on the next page then before proceeding you must contact CitiPower/Powercor to determine if a **PERMIT TO WORK** is required and to organise a **SITE VISIT**

Site Visit/Permit To Work applications may be lodged at:

https://www.citipower.com.au/working-with-us/suppliers/online-permit-applications/site-visit/

If you need assistance to determine if you need a Site Visit please call:



CitiPower on 1300 301 101



Powercor on 132 206

Underground Electricity Asset Location Details Accuracy:

The Underground Electricity asset location details provided with this response are based on the best information available at the time

All reasonable care has been taken to ensure the accuracy of the information provided but complete accuracy cannot be guaranteed

Please be aware that the Underground Electricity Asset depths shown on the attached plans are accurate at the time of recording, however, due to works undertaken over the years by parties other than CitiPower/Powercor the Underground Electricity Asset depths may differ to those shown on the plans

Contact with Underground Electricity Cables can cause serious injury or death

If you observe any Underground Electricity Assets that do not appear on the records provided

Stop Work Immediately

and contact CitiPower/Powercor on the above numbers

UNDERGROUND ELECTRICITY HAZARD AWARENESS INSTRUCTIONS

For CitiPower & Powercor Dial Before You Dig customers

EXCLUSION ZONES



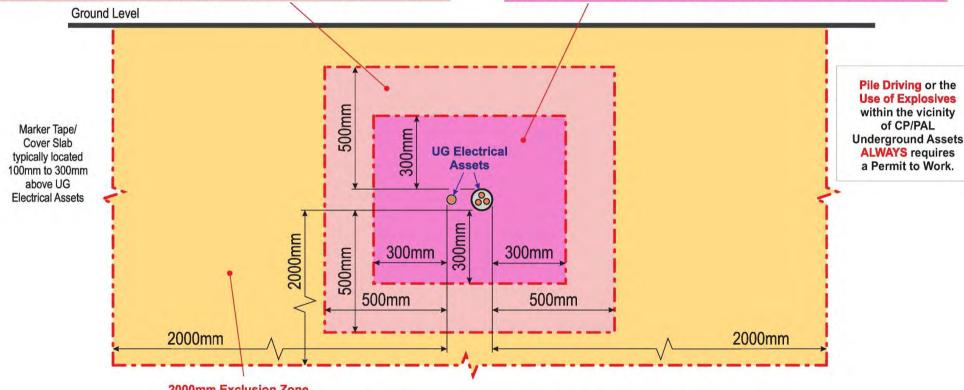


500mm Exclusion Zone
Heavy Machinery & Mechanical Excavation

Heavy (Crawler Type) Machinery operation and Mechanical Excavation within a 500mm distance of Underground Electricity Assets requires a Permit to Work

300mm Exclusion Zone Hand Tools Only

All Excavation within a 300mm distance of Underground Electricity Assets requires a Permit to Work and must only be performed with Hand Tools



2000mm Exclusion Zone

Works within this area that require a Site Technical Assessment and may require a Permit to Work includes:

Pot Hole Boring Machine (Vertical Boring), Directional Boring Machine, Excavations Parallel to Underground Electricity Assets, Excavations Across Underground Electricity Assets

For Underground Electricity Asset location purposes:

Careful Excavation by hand may be performed under a Permit to Work above energised Underground Electricity Assets within the Exclusion Zone Excavation must cease once either Marker Tape, Cover Slab or top of asset is located. All excavation must be performed BY HAND using only non-powered tools No disturbance of the Marker Tape, the Protective Cover or the Asset is allowed. Any disturbance must be reported immediately to CitiPower/Powercor

Excavation Below Underground Electricity Assets:

All excavation BELOW Underground Electricity Assets outside of the Exclusion Zone must ensure that there is no disturbance to the asset and that the area is restored to full pre-excavation integrity upon reinstatement





Dial Before You Dig (DBYD) Electrical Asset Location Information

CitiPower/Powercor

Locked Bag 14090, Melbourne VIC 8001

General Enquiries Telephone: 132 206

To: ('Enquirer')

Jasmine Walters

338a Carrington Street

Adelaide SA 5000

Enquiry Details	
Utility ID	50024
Sequence Number	257040419
Enquiry Date	25/06/2025
Response	ALL CLEAR
Address	Redlands 5721b Sturt Hwy
	Monak, NSW 2738
Location in Road	
Activity	Planning & Design

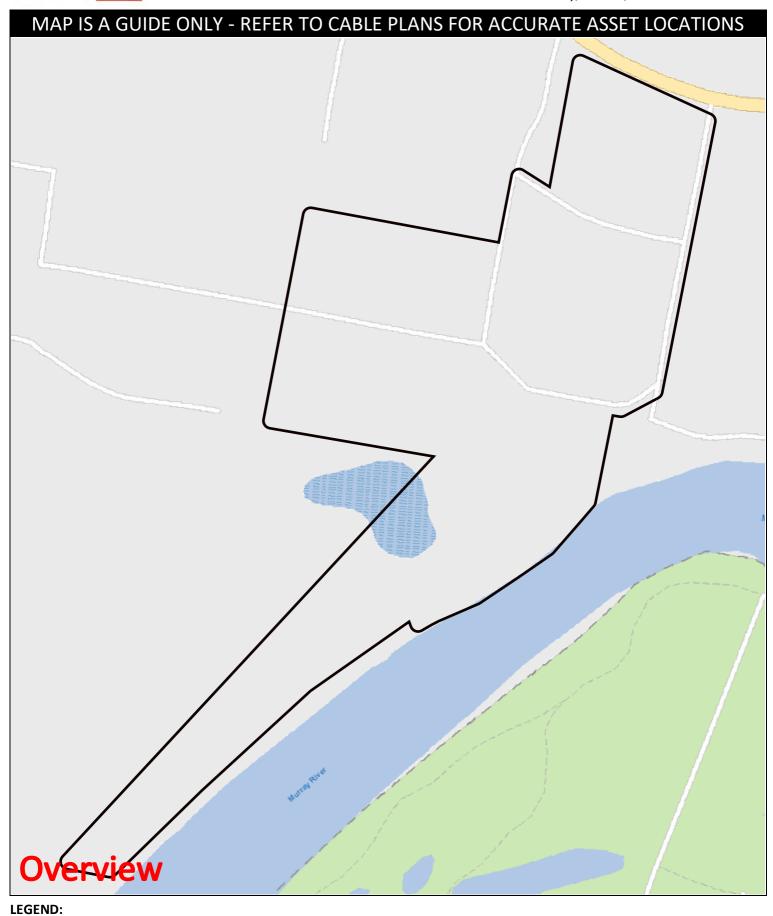
Enquirer Details	
Customer ID	3600898
Contact	Jasmine Walters
Company	MasterPlan Pty Ltd
Email	qe2vck1mnp9877.drsmm5nta8n1jj@smarterwx-mail.byda.com.au
Phone	+61881935600

Enquirer Responsibilities

This notification is valid for 28 days from the issue date. CitiPower/Powercor assets are critical infrastructure and great care must be taken to avoid asset damage and risk to public safety. The information supplied in the DBYD Response is intended to be indicative only. External parties should make their own enquiries to ensure the accuracy of the information, including but not limited to:

- Check that the location of the dig site indicated is correct, if not you must submit a new enquiry.
- Should your scope of works change or the plan validity dates expire, you must submit a new enquiry.
- If you do not understand the plans provided please contact CitiPower/Powercor prior to works commencing.
- Always perform an onsite inspection to establish the presence of assets.
- Ensure you adhere to any State legislative requirements regarding Duty of Care and safe digging requirements.

Report any asset damage immediately on 132 206. Note: CitiPower/Powercor reserves the right to recover compensation for damages.



Communication Cable

- Earth Cable

This map represents the location of the submitted BYDA Work Area and all Citipower/Powercor responses are based on this location. It is the responsibility of the enquirer to ensure the accuracy of the BYDA Work Area.

High Voltage Cable

Low Voltage Cable

BYDA Work Area

Zone Substation

Scale: 1:5000

Pole

SWER Substation

O Distribution Substation



Telstra VICTAS

Referral 257040420

Member Phone 1800 653 935

Responses from this member

Response received Wed 25 Jun 2025 4.00pm

Page
20
22
24
Excluded
25

Attention: Jasmine Walters

Site Location: Redlands 5721b Sturt Hwy, Monak, NSW 2738

Your Job Reference: Redlands 5721b Sturt Hwy

Please do not reply to this email, this is an automated message -

Thank you for requesting Telstra information via Before You Dig Australia (BYDA).

This response contains Telstra information relating to your recent BYDA request.

Please refer to all enclosed attachments for more information.

Information for opening Telstra Asset Plans as well as some other useful contact information is noted in the attached documents.

Report Damage to Telstra Equipment: Report damages to Telstra equipment - Telstra

Please note:

When working in the vicinity of telecommunications plant you have a 'Duty of Care' that must be observed.

Ensure you read all documents (attached) - they contain important information.

Please also refer to the **Before you Dig Australia - BEST PRACTISE GUIDES and The five Ps of safe excavation** https://www.byda.com.au/before-you-dig/best-practice-guides/, The essential steps that must be undertaken prior to commencing construction activities.

WARNING - MAJOR CABLES and/or OPTIC FIBRE IN THE AREA.

Phone 1800 653 935 for further assistance.

Note: In some areas Telstra fibre routes may be marked as "Amcom", as Telstra has purchased much of this infrastructure. If in doubt, please contact Telstra Plan services on the number above. Telstra plans and information are only valid for 60 days from the date of issue.

WARNING:

Telstra plans and location information conform to Quality Level 'D' of the Australian Standard AS 5488 - Classification of Subsurface Utility Information. As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D. Refer to AS 5488 for further details. The exact position of Telstra assets can only be validated by physically exposing them. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy. Further on site investigation is required to validate the exact location of Telstra assets prior to commencing work. A Certified Locating Organisation is an essential part of the process to validate the exact location of Telstra assets and to ensure the assets are protected during construction works. See the **Before You Dig Australia - BEST PRACTISE GUIDES and The five Ps of safe excavation**

https://www.byda.com.au/before-you-dig/best-practice-guides/.

Please note that:

- it is a criminal offence under the *Criminal Code Act* 1995 (Cth) to tamper or interfere with telecommunications infrastructure.
- Telstra will take action to recover compensation for damage caused to property and assets, and for interference with the operation of Telstra's networks and customers' services.

Telstra's plans contain Telstra's confidential information and are provided on the basis that they are used solely for identifying the location or vicinity of Telstra's infrastructure to avoid damage to this infrastructure occurring as part of any digging or other excavation activity. You must not use Telstra's plans for any other purpose or in a way that will cause Telstra loss or damage and you must comply with any other terms of access to the data that have been provided to you by Telstra (including Conditions of Use or Access).

(See attached file: Telstra Duty of Care v32.0c.pdf)

(See attached file: Telstra Map Legend 4.0b.pdf)

Disclaimer and legal details



*Telstra advises that the accuracy of the information provided by Telstra conforms to Quality Level D as defined in AS5488-2013.

It is a criminal offence under the Criminal Code Act 1995 (Cth) to tamper or interfere with telecommunications infrastructure.

Telstra will also take action to recover costs and damages from persons who damage assets or interfere with the operation of **Telstra's** networks.

By receiving this information including the indicative plans that are provided as part of this information package you confirm that you understand and accept the risks of working near **Telstra's** network and the importance of taking all the necessary steps to confirm the presence, alignments and various depths of **Telstra's** network. This in addition to, and not in replacement of, any duties and obligations you have under applicable law.

When working in the vicinity of a telecommunications plant you have a "Duty of Care" that must be observed. Please read and understand all the information and disclaimers provided below.

The Telstra network is complex and requires expert knowledge to interpret information, to identify and locate components, to pothole underground assets for validation and to safely work around assets without causing damage. If you are not an expert and/or qualified in these areas, then you must not attempt these activities. Telstra will seek compensation for damages caused to its property and losses caused to Telstra and its customers. Construction activities and/or any activities that potentially may impact on Telstra's assets must not commence without first undertaking these steps. Construction activities can include anything that involves breaking ground, potentially affecting Telstra assets.

If you are designing a project, it is recommended that you also undertake these steps to validate underground assets prior to committing to your design.

This Notice has been provided as a guide only and may not provide you with all the information that is required for you to determine what assets are on or near your site of interest. You will also need to collate and understand all information received from other Utilities and understand that some Utilities are not a part of the BYDA program and make your own enquiries as appropriate. It is the responsibility of the entities undertaking the works to protect **Telstra's** network during excavation / construction works.

Telstra owns and retains the copyright in all plans and details provided in conjunction with the applicant's request. The applicant is authorised to use the plans and details only for the purpose indicated in the applicant's request. The applicant must not use the plans or details for any other purpose.

Telstra plans or other details are provided only for the use of the applicant, its servants, agents, or CERTLOC Certified Locating Organisation (CLO). The applicant must not give the plans or details to any parties other than these and must not generate profit from commercialising the plans or details.

Telstra, its servants or agents shall not be liable for any loss or damage caused or occasioned by the use of plans and or details so supplied to the applicant, its servants and agents, and the applicant agrees to indemnify Telstra against any claim or demand for any such loss or damage.

Please ensure Telstra plans and information provided always remains on-site throughout the inspection, location, and construction phase of any works.

Telstra plans are valid for 60 days after issue and must be replaced if required after the 60 days.

Data Extraction Fees

In some instances, a data extraction fee may be applicable for the supply of Telstra information. Typically, a data extraction fee may apply to large projects, planning and design requests or requests to be supplied in non-standard formats. For further details contact Telstra Location Intelligence Team.

Telstra does not accept any liability or responsibility for the performance of or advice given by a CERTLOC Certified Locating Organisation (CLO). Certification is an initiative taken by Telstra towards the establishment and maintenance of competency standards. However, performance and the advice given will always depend on the nature of the individual engagement.

Neither the Certified Locating Organisation nor any of its employees are an employee or agent for Telstra. Telstra is not liable for any damage or loss caused by the Certified Locating Organisation or its employees.

Once all work is completed, the excavation should be reinstated with the same type of excavated material unless specified by Telstra.

The information contained within this pamphlet must be used in conjunction with other material supplied as part of this request for information to adequately control the risk of potential asset damage.

When using excavators and other machinery, also check the location of overhead power lines.

Workers and equipment must maintain safety exclusion zones around power lines

WARNING: Telstra plans and location information conform to Quality Level 'D' of the Australian Standard AS 5488 - Classification of Subsurface Utility Information. As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D. Refer to AS 5488 for further details. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy shown on the plans. FURTHER ON SITE INVESTIGATION IS REQUIRED TO VALIDATE THE EXACT LOCATION OF TELSTRA PLANT PRIOR TO COMMENCING CONSTRUCTION WORK. A plant location service is an essential part of the process to validate the exact location of Telstra assets and to ensure the assets are protected during construction works. The exact position of Telstra assets can only be validated by physically exposing them. Telstra will seek compensation for damages caused to its property and losses caused to Telstra and its customers.

Privacy Note

Your information has been provided to Telstra by BYDA to enable Telstra to respond to your BYDA request. Telstra keeps your information in accordance with its privacy statement. You can obtain a copy at www.telstra.com.au/privacy or by calling us at 1800 039 059 (business hours only).

General Information



Before you Dig Australia - BEST PRACTISE GUIDES

The five Ps of safe excavation

https://www.byda.com.au/before-you-dig/best-practice-guides/

OPENING ELECTRONIC MAP ATTACHMENTS -

Telstra Cable Plans are generated automatically in either PDF or DWF file types.

Dependent on the site address and the size of area selected. You may need to download and install free viewing software from the internet e.g.



DWF Map Files (all sizes over A3)

Autodesk Viewer (Internet Browser) https://viewer.autodesk.com/ or Autodesk Design Review http://usa.autodesk.com/design-review/ for DWF files. (Windows PC)



PDF Map Files (max size A3)

Adobe Acrobat Reader http://get.adobe.com/reader/



Telstra BYDA map related enquiries email Telstra.Plans@team.telstra.com 1800 653 935 (AEST Business Hours only)



REPORT ANY DAMAGE TO THE TELSTRA NETWORK IMMEDIATELY

Report online - https://www.telstra.com.au/forms/report-damage-to-telstraequipment

Ph: 13 22 03

If you receive a message asking for a phone or account number say:

"I don't have one" then say "Report Damage" then press 1 to speak to an operator.



Telstra New Connections / Disconnections 13 22 00



Telstra asset relocation enquiries: 1800 810 443 (AEST business hours only).

NetworkIntegrity@team.telstra.com

https://www.telstra.com.au/consumer-advice/digging-construction



Telstra Aerial Assets Group (overhead network) 1800 047 909

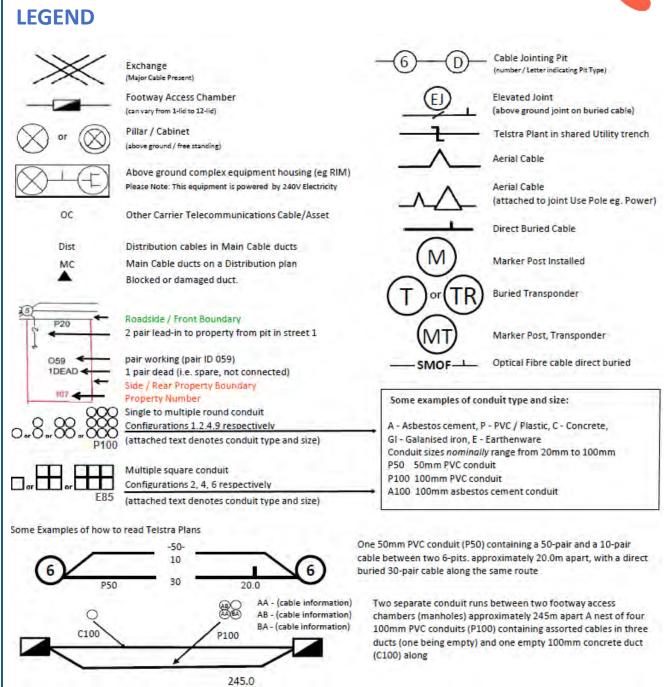


CERTLOC Certified Locating Organisation (CLO)

certloc.com.au/locators/

Only Telstra authorised personnel and CERTLOC Locators can access Telstra's Pit and Pipe Network.





Protect our Network:

by maintaining the following distances from our assets:

- 1.0m Mechanical Excavators, Farm Ploughing, Tree Removal
- 500mmVibrating Plate or Wacker Packer Compactor
- 600mm Heavy Vehicle Traffic (over 3 tonnes) not to be driven across Telstra ducts or plant.
- 1.0mJackhammers/Pneumatic Breakers
- 2.0m Boring Equipment (in-line, horizontal and vertical)

For more info contact a <u>CERTLOC Certified Locating Organisation (CLO)</u> or Telstra Location Intelligence Team 1800 653 935

5758 Sturt Hwy



Review responses online >



Received 3 of 3 responses All responses received

5758 Sturt Hwy, Monak NSW 2738

Job dates 01/11/2025 → 31/12/2025

These plans expire on 2 Oct 2025

Lodged by Jasmine Walters

Authority	Status	Page
☑ BYDA Confirmation		2
Essential Energy	Received	4
⊪ Powercor - Mildura	Received	13
⊪ Telstra VICTAS	Received	19

Zero damage - Zero harm - Zero disruption

Contact Details

 Contact
 Contact number
 Company
 Enquirer ID

 Jasmine Walters
 (08) 8193 5600
 MasterPlan Pty Ltd
 3600898

Email

jasminew@masterplan.com.au

Address

338a Carrington Street Adelaide SA 5000

Job Site and Enquiry Details

WARNING: The map below only displays the location of the proposed job site and does not display any asset owners' pipe or cables. The area highlighted has been used only to identify the participating asset owners, who will send information to you directly.

Enquiry date	Start date	End date	On behalf of	Job purpose	Locations	Onsite activities
04/09/2025	01/11/2025	31/12/2025	Private	Design	Private	Planning & Design



Check that the location of the job site is correct. If not, you must submit a new enquiry.

If the scope of works change or plan validity dates expire, you must submit a new enquiry.

Do NOT dig without plans. Safe excavation is your responsibility. If you don't understand the plans or how to proceed safely, please contact the relevant asset owners.

User Reference 5758 Sturt Hwy Address 5758 Sturt Hwy Monak NSW 2738 Notes/description

-

Your Responsibility and Duty of Care

- Lodging an enquiry does not authorise project commencement. Before starting work, you must obtain all necessary information from all affected asset owners.
- If you don't receive plans within 2 business days, contact the asset owner & quote their sequence number.
- Always follow the 5Ps of Safe Excavation (page 2), and locate assets before commencing work.
- Ensure you comply with State legislative requirements for Duty of Care and safe digging.
- If you damage an underground asset, you MUST advise the asset owner immediately.
- By using the BYDA service, you agree to the Privacy Policy and Term of Use.
- For more information on safe digging practices, visit www.byda.com.au

Asset Owner Details

Below is a list of asset owners with underground infrastructure in and around your job site. It is your responsibility to identify the presence of these assets. Plans issued by Members are indicative only unless specified otherwise. Note: not all asset owners are registered with BYDA. You must contact asset owners not listed here directly.

Referral ID (Seq. no)	Authority Name	Phone	Status
260644907	Essential Energy	13 23 91	NOTIFIED
260644908	Powercor - Mildura	13 22 06	NOTIFIED
260644909	Telstra VICTAS	1800 653 935	NOTIFIED

END OF UTILITIES LIST



Plan

Plan your job. Use the BYDA service at least one day before your job is due to begin, and ensure you have the correct plans and information required to carry out a safe project.



Prepare

Prepare by communicating with asset owners if you need assistance. Look for clues onsite. Engage a skilled Locator.



Pothole

Potholing is physically sighting the asset by hand digging or hydro vacuum extraction.



Protect

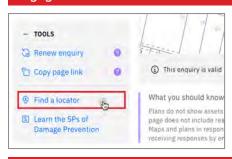
Protecting and supporting the exposed infrastructure is the responsibility of the excavator. Always erect safety barriers in areas of risk and enforce exclusion zones.



Proceed

Only proceed with your excavation work after planning, preparing, potholing (unless prohibited), and having protective measures in place.

Engage a skilled Locator



When you lodge an enquiry you will see skilled Locators to contact

Visit the Certified Locator website directly and search for a locator near you

certloc.com.au/locators

Get FREE Quotes for Contractors & Equipment Fast



Use iseekplant's FREE marketplace to get quotes for the equipment or services you need on your project. Compare quotes from trusted local contractors and get your project done on time and in budget.

- 1. Fill out your job details in our FREE quick quote form.
- 2. We send the request to trusted local contractors.
- 3. The local contractors will contact you directly with quotes

GET QUOTE

Use iseekplant to find trusted contractors near you today, visit: blog.iseekplant.com.au/byda-isp-get-quotes

Book a FREE BYDA Session



BYDA offers free training sessions to suit you and your organisation's needs covering safe work practices when working near essential infrastructure assets. The free sessions are offered in two different formats online and face-to-face.

To book a session, visit:

byda.com.au/contact/education-awareness-enquiry-form

BOOK NOW

Essential Energy

Referral 260644907

Member Phone 13 23 91

Responses from this member

Response received Thu 4 Sep 2025 1.47pm

File name	Page
Response Body	5
EW_ASSETS_FOUNDsafetyNotice.pdf	6
Coversheet_EW_ASSETS_FOUND.pdf	10
plot1610638510380178261818.pdf	12

Asset Name: 50215

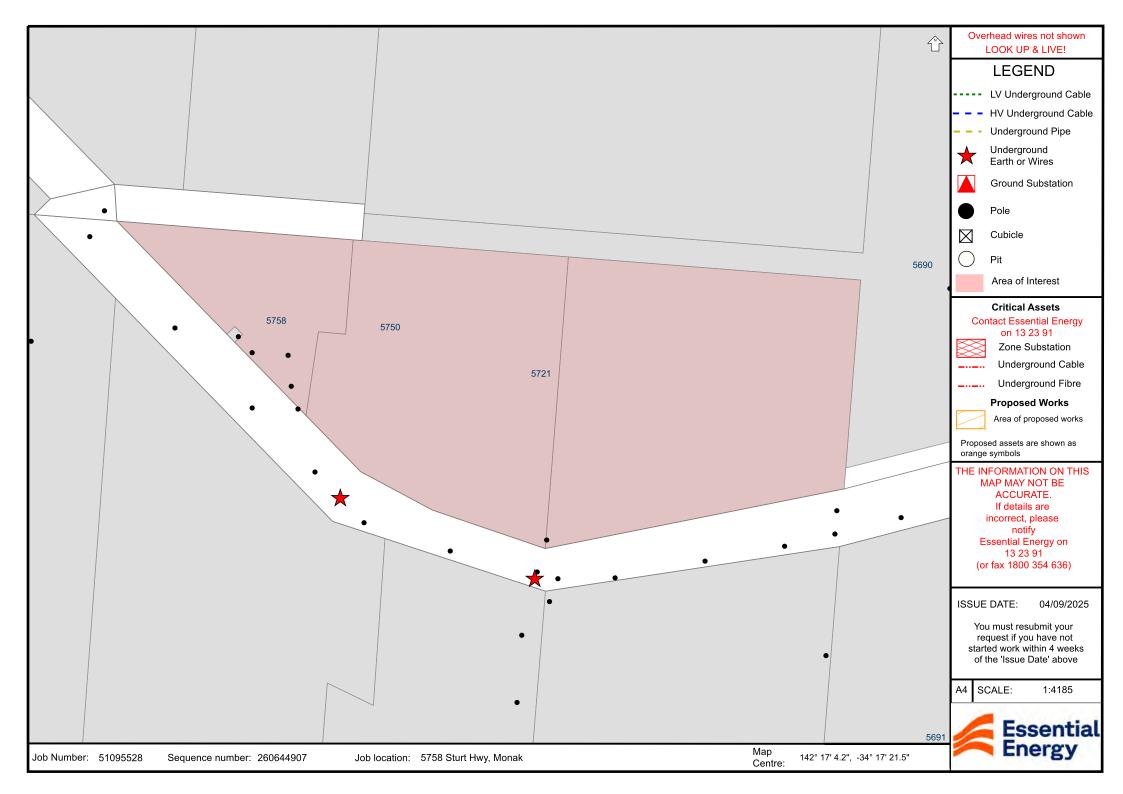
Date of enquiry: 4/09/2025 2:15:00 PM Notification No: 51095528 (Job No)

Sequence No: 260644907

Customer's Name: Jasmine Walters Customer's Phone No: +61881935600

Address supplied for dig site location 5758 Sturt Hwy, Monak, NSW

You will require a PDF viewer such as Adobe Acrobat Reader to view the attached documents. Adobe Acrobat Reader is freely available at http://get.adobe.com/reader/.



Referral Member Phone 260644908 13 22 06

Responses from this member

Response received Thu 4 Sep 2025 4.02pm

File name	Page
Response Body	14
260644908 - Citipower Powercor Overview Plan.pdf	15
CitiPower Powercor UG Electricity Hazard Awareness Instructions.pdf	16
260644908 - Citipower Powercor Response letter.pdf	18

This referral has been successfully processed by CitiPower Ltd / Powercor Australia Ltd and the results are contained in the attached files.

Understanding your DBYD Response Files

- Read the "260644908 Citipower Powercor Response letter.pdf" and the "CitiPower Powercor UG Electricity Hazard Awareness Instructions.pdf" documents for an overview of your impact on CitiPower/Powercor assets and your obligations
- The remaining (PDF) attachments are detailed construction drawings within your area of works.
- Attachments over 13MB are split into multiple emails (eg. Part 1 of X) ensure you have all documents

Please DO NOT REPLY TO THIS EMAIL as it has been automatically generated and replies are not monitored.

Sequence No: 260644908 Date: 04 Sep 2025

Enquirer: MasterPlan Pty Ltd Contact: Jasmine Walters

Email: qe2vck1mnp9877.j03vp9y77kkiqk@smarterwx-mail.byda.com.au

Phone: +61881935600

Address: 338a Carrington Street, Adelaide SA

Site Address: 5758 Sturt Hwy, Monak NSW

Activity: Planning & Design

Job Number: 51095528

If you require assistance, clarification or Permit to Works please contact 132 206.

We thank you for your enquiry and appreciate your continued use of the "Dial Before You Dig" service.





260644908

5758 Sturt Hwy, Monak, NSW 2738

MAP IS A GUIDE ONLY - REFER TO CABLE PLANS FOR ACCURATE ASSET LOCATIONS Sturt Highway **Overview LEGEND:**

- Communication Cable

- Earth Cable

This map represents the location of the submitted BYDA Work Area and all Citipower/Powercor responses are based on this location. It is the responsibility of the enquirer to ensure the accuracy of the BYDA Work Area.

High Voltage Cable

Low Voltage Cable

BYDA Work Area

Zone Substation

Scale: 1:5000

Pole

HV Pits

SWER Substation

O Distribution Substation



UNDERGROUND ELECTRICITY HAZARD AWARENESS INSTRUCTIONS





For CitiPower & Powercor Dial Before You Dig customers

Always complete a Dial Before You Dig request before you proceed with any work plans



If there are Underground Electricity assets identified within your work area please ensure that you carefully evaluate all of the information provided

If any part of your proposed works impacts on the **EXCLUSION ZONES** shown on the next page then before proceeding you must contact CitiPower/Powercor to determine if a **PERMIT TO WORK** is required and to organise a **SITE VISIT**

Site Visit/Permit To Work applications may be lodged at:

https://www.citipower.com.au/working-with-us/suppliers/online-permit-applications/site-visit/

If you need assistance to determine if you need a Site Visit please call:



CitiPower on 1300 301 101



Powercor on 132 206

Underground Electricity Asset Location Details Accuracy:

The Underground Electricity asset location details provided with this response are based on the best information available at the time

All reasonable care has been taken to ensure the accuracy of the information provided but complete accuracy cannot be guaranteed

Please be aware that the Underground Electricity Asset depths shown on the attached plans are accurate at the time of recording, however, due to works undertaken over the years by parties other than CitiPower/Powercor the Underground Electricity Asset depths may differ to those shown on the plans

Contact with Underground Electricity Cables can cause serious injury or death

If you observe any Underground Electricity Assets that do not appear on the records provided

Stop Work Immediately

and contact CitiPower/Powercor on the above numbers

UNDERGROUND ELECTRICITY HAZARD AWARENESS INSTRUCTIONS

For CitiPower & Powercor Dial Before You Dig customers

EXCLUSION ZONES



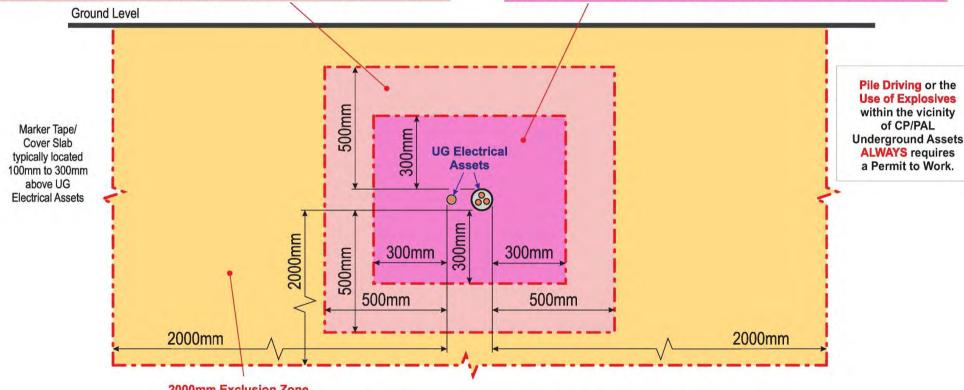


500mm Exclusion Zone
Heavy Machinery & Mechanical Excavation

Heavy (Crawler Type) Machinery operation and Mechanical Excavation within a 500mm distance of Underground Electricity Assets requires a Permit to Work

300mm Exclusion Zone Hand Tools Only

All Excavation within a 300mm distance of Underground Electricity Assets requires a Permit to Work and must only be performed with Hand Tools



2000mm Exclusion Zone

Works within this area that require a Site Technical Assessment and may require a Permit to Work includes:

Pot Hole Boring Machine (Vertical Boring), Directional Boring Machine, Excavations Parallel to Underground Electricity Assets, Excavations Across Underground Electricity Assets

For Underground Electricity Asset location purposes:

Careful Excavation by hand may be performed under a Permit to Work above energised Underground Electricity Assets within the Exclusion Zone Excavation must cease once either Marker Tape, Cover Slab or top of asset is located. All excavation must be performed BY HAND using only non-powered tools No disturbance of the Marker Tape, the Protective Cover or the Asset is allowed. Any disturbance must be reported immediately to CitiPower/Powercor

Excavation Below Underground Electricity Assets:

All excavation BELOW Underground Electricity Assets outside of the Exclusion Zone must ensure that there is no disturbance to the asset and that the area is restored to full pre-excavation integrity upon reinstatement





Dial Before You Dig (DBYD) Electrical Asset Location Information

CitiPower/Powercor

Locked Bag 14090, Melbourne VIC 8001

General Enquiries Telephone: 132 206

To: ('Enquirer')

Jasmine Walters

338a Carrington Street

Adelaide SA 5000

Enquiry Details	
Utility ID	50024
Sequence Number	260644908
Enquiry Date	04/09/2025
Response	ALL CLEAR
Address	5758 Sturt Hwy
	Monak, NSW 2738
Location in Road	
Activity	Planning & Design

Enquirer Details		
Customer ID	3600898	
Contact	Jasmine Walters	
Company	MasterPlan Pty Ltd	
Email	qe2vck1mnp9877.j03vp9y77kkiqk@smarterwx-mail.byda.com.au	
Phone	+61881935600	

Enquirer Responsibilities

This notification is valid for 28 days from the issue date. CitiPower/Powercor assets are critical infrastructure and great care must be taken to avoid asset damage and risk to public safety. The information supplied in the DBYD Response is intended to be indicative only. External parties should make their own enquiries to ensure the accuracy of the information, including but not limited to:

- Check that the location of the dig site indicated is correct, if not you must submit a new enquiry.
- Should your scope of works change or the plan validity dates expire, you must submit a new enquiry.
- If you do not understand the plans provided please contact CitiPower/Powercor prior to works commencing.
- Always perform an onsite inspection to establish the presence of assets.
- Ensure you adhere to any State legislative requirements regarding Duty of Care and safe digging requirements.

Report any asset damage immediately on 132 206. Note: CitiPower/Powercor reserves the right to recover compensation for damages.

Telstra VICTAS

Referral 260644909

Member Phone 1800 653 935

Responses from this member

Response received Thu 4 Sep 2025 1.53pm

File name	Page
Response Body	
AccreditedPlantLocators 2025-01-08a.pdf	
260644909.pdf	23
Telstra Duty of Care v32.0c.pdf	
Telstra Map Legend 4.0b.pdf	

Attention: Jasmine Walters

Site Location: 5758 Sturt Hwy, Monak, NSW 2738

Your Job Reference: 5758 Sturt Hwy

Please do not reply to this email, this is an automated message -

Thank you for requesting Telstra information via Before You Dig Australia (BYDA).

This response contains Telstra information relating to your recent BYDA request.

Please refer to all enclosed attachments for more information.

Information for opening Telstra Asset Plans as well as some other useful contact information is noted in the attached documents.

Report Damage to Telstra Equipment: Report damages to Telstra equipment - Telstra

Please note:

When working in the vicinity of telecommunications plant you have a 'Duty of Care' that must be observed.

Ensure you read all documents (attached) - they contain important information.

Please also refer to the **Before you Dig Australia - BEST PRACTISE GUIDES and The five Ps of safe excavation** https://www.byda.com.au/before-you-dig/best-practice-guides/, The essential steps that must be undertaken prior to commencing construction activities.

WARNING - MAJOR CABLES and/or OPTIC FIBRE IN THE AREA.

Phone 1800 653 935 for further assistance.

Note: In some areas Telstra fibre routes may be marked as "Amcom", as Telstra has purchased much of this infrastructure. If in doubt, please contact Telstra Plan services on the number above. Telstra plans and information are only valid for 60 days from the date of issue.

WARNING:

Telstra plans and location information conform to Quality Level 'D' of the Australian Standard AS 5488 - Classification of Subsurface Utility Information. As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D. Refer to AS 5488 for further details. The exact position of Telstra assets can only be validated by physically exposing them. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy. Further on site investigation is required to validate the exact location of Telstra assets prior to commencing work. A Certified Locating Organisation is an essential part of the process to validate the exact location of Telstra assets and to ensure the assets are protected during construction works. See the **Before You Dig Australia - BEST PRACTISE GUIDES and The five Ps of safe excavation**

https://www.byda.com.au/before-you-dig/best-practice-guides/.

Please note that:

- it is a criminal offence under the *Criminal Code Act* 1995 (Cth) to tamper or interfere with telecommunications infrastructure.
- Telstra will take action to recover compensation for damage caused to property and assets, and for interference with the operation of Telstra's networks and customers' services.

Telstra's plans contain Telstra's confidential information and are provided on the basis that they are used solely for identifying the location or vicinity of Telstra's infrastructure to avoid damage to this infrastructure occurring as part of any digging or other excavation activity. You must not use Telstra's plans for any other purpose or in a way that will cause Telstra loss or damage and you must comply with any other terms of access to the data that have been provided to you by Telstra (including Conditions of Use or Access).

(See attached file: Telstra Duty of Care v32.0c.pdf)

(See attached file: Telstra Map Legend 4.0b.pdf)

General Information



Before you Dig Australia - BEST PRACTISE GUIDES

The five Ps of safe excavation

https://www.byda.com.au/before-you-dig/best-practice-guides/

OPENING ELECTRONIC MAP ATTACHMENTS -

Telstra Cable Plans are generated automatically in either PDF or DWF file types.

Dependent on the site address and the size of area selected. You may need to download and install free viewing software from the internet e.g.



DWF Map Files (all sizes over A3)

Autodesk Viewer (Internet Browser) https://viewer.autodesk.com/ or Autodesk Design Review http://usa.autodesk.com/design-review/ for DWF files. (Windows PC)



PDF Map Files (max size A3)

Adobe Acrobat Reader http://get.adobe.com/reader/



Telstra BYDA map related enquiries email Telstra.Plans@team.telstra.com 1800 653 935 (AEST Business Hours only)



REPORT ANY DAMAGE TO THE TELSTRA NETWORK IMMEDIATELY

Report online - https://www.telstra.com.au/forms/report-damage-to-telstraequipment

Ph: 13 22 03

If you receive a message asking for a phone or account number say:

"I don't have one" then say "Report Damage" then press 1 to speak to an operator.



Telstra New Connections / Disconnections 13 22 00



Telstra asset relocation enquiries: 1800 810 443 (AEST business hours only).

NetworkIntegrity@team.telstra.com

https://www.telstra.com.au/consumer-advice/digging-construction



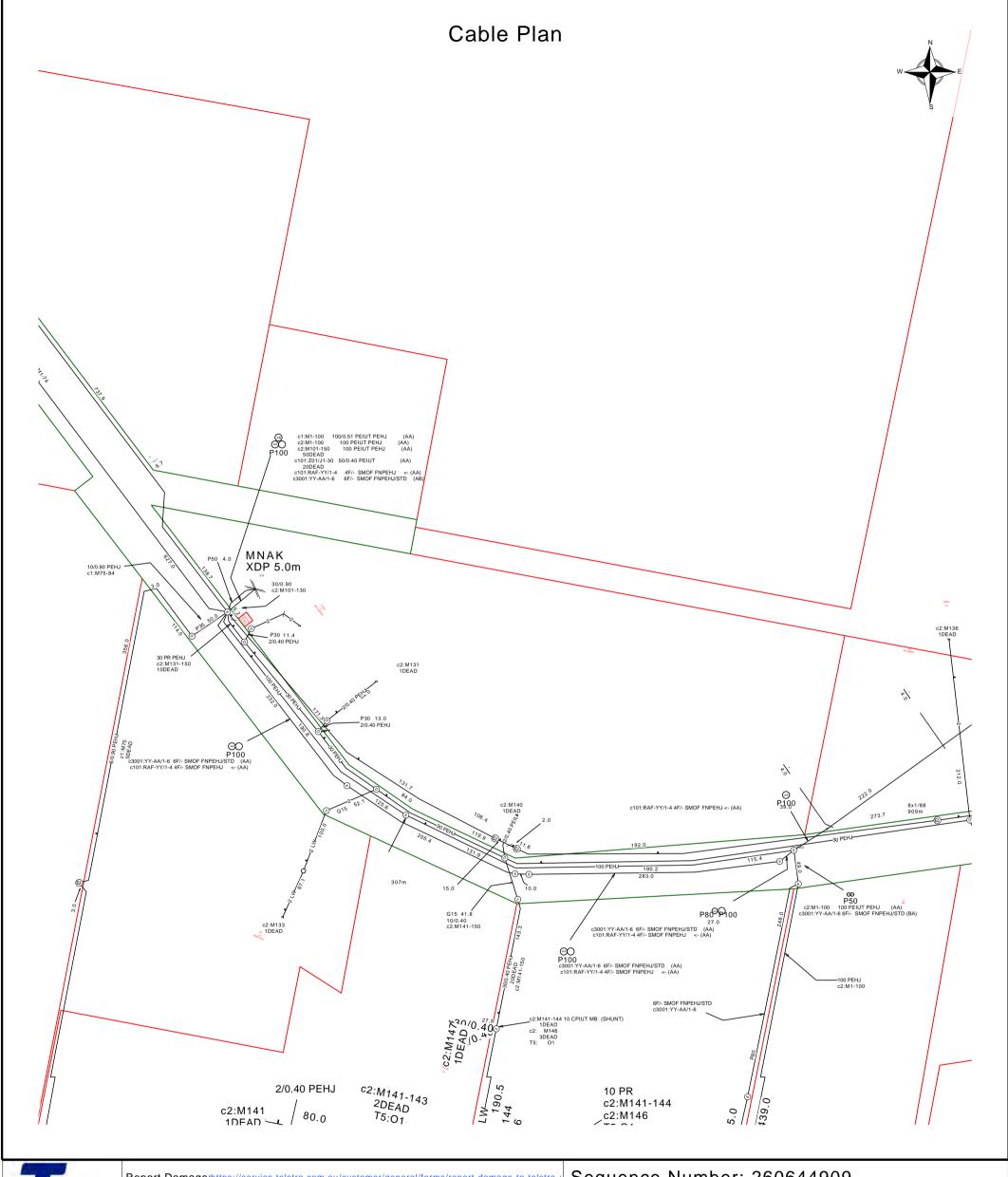
Telstra Aerial Assets Group (overhead network) 1800 047 909



CERTLOC Certified Locating Organisation (CLO)

certloc.com.au/locators/

Only Telstra authorised personnel and CERTLOC Locators can access Telstra's Pit and Pipe Network.





Report Damage:https://service.telstra.com.au/customer/general/forms/report-damage-to-telstra-Ph - 13 22 03

Email - Telstra.Plans@team.telstra.com

Planned Services - ph 1800 653 935 (AEST bus hrs only) General Enquiries

TELSTRA LIMITED A.C.N. 086 174 781

Generated On 04/09/2025 14:21:35

Sequence Number: 260644909

CAUTION: Fibre optic and/ or major network present in plot area. Please read the Duty of Care and contact Telstra Plan Services should you require any assistance.

WARNING

Telstra plans and location information conform to Quality Level "D" of the Australian Standard AS 5488-Classification of Subsurface Utility Information.

As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D.

Refer to AS 5488 for further details. The exact position of Telstra assets can only be validated by physically exposing it.

Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy.

Further on site investigation is required to validate the exact location of Telstra plant prior to commencing construction work. A Certified Locating Organisation is an essential part of the process to validate the exact location of Telstra assets and to ensure the asset is protected during construction works.

See the Steps- Telstra Duty of Care that was provided in the email response.

Disclaimer and legal details



*Telstra advises that the accuracy of the information provided by Telstra conforms to Quality Level D as defined in AS5488-2013.

It is a criminal offence under the Criminal Code Act 1995 (Cth) to tamper or interfere with telecommunications infrastructure.

Telstra will also take action to recover costs and damages from persons who damage assets or interfere with the operation of **Telstra's** networks.

By receiving this information including the indicative plans that are provided as part of this information package you confirm that you understand and accept the risks of working near **Telstra's** network and the importance of taking all the necessary steps to confirm the presence, alignments and various depths of **Telstra's** network. This in addition to, and not in replacement of, any duties and obligations you have under applicable law.

When working in the vicinity of a telecommunications plant you have a "Duty of Care" that must be observed. Please read and understand all the information and disclaimers provided below.

The Telstra network is complex and requires expert knowledge to interpret information, to identify and locate components, to pothole underground assets for validation and to safely work around assets without causing damage. If you are not an expert and/or qualified in these areas, then you must not attempt these activities. Telstra will seek compensation for damages caused to its property and losses caused to Telstra and its customers. Construction activities and/or any activities that potentially may impact on Telstra's assets must not commence without first undertaking these steps. Construction activities can include anything that involves breaking ground, potentially affecting Telstra assets.

If you are designing a project, it is recommended that you also undertake these steps to validate underground assets prior to committing to your design.

This Notice has been provided as a guide only and may not provide you with all the information that is required for you to determine what assets are on or near your site of interest. You will also need to collate and understand all information received from other Utilities and understand that some Utilities are not a part of the BYDA program and make your own enquiries as appropriate. It is the responsibility of the entities undertaking the works to protect **Telstra's** network during excavation / construction works.

Telstra owns and retains the copyright in all plans and details provided in conjunction with the applicant's request. The applicant is authorised to use the plans and details only for the purpose indicated in the applicant's request. The applicant must not use the plans or details for any other purpose.

Telstra plans or other details are provided only for the use of the applicant, its servants, agents, or CERTLOC Certified Locating Organisation (CLO). The applicant must not give the plans or details to any parties other than these and must not generate profit from commercialising the plans or details.

Telstra, its servants or agents shall not be liable for any loss or damage caused or occasioned by the use of plans and or details so supplied to the applicant, its servants and agents, and the applicant agrees to indemnify Telstra against any claim or demand for any such loss or damage.

Please ensure Telstra plans and information provided always remains on-site throughout the inspection, location, and construction phase of any works.

Telstra plans are valid for 60 days after issue and must be replaced if required after the 60 days.

Data Extraction Fees

In some instances, a data extraction fee may be applicable for the supply of Telstra information. Typically, a data extraction fee may apply to large projects, planning and design requests or requests to be supplied in non-standard formats. For further details contact Telstra Location Intelligence Team.

Telstra does not accept any liability or responsibility for the performance of or advice given by a CERTLOC Certified Locating Organisation (CLO). Certification is an initiative taken by Telstra towards the establishment and maintenance of competency standards. However, performance and the advice given will always depend on the nature of the individual engagement.

Neither the Certified Locating Organisation nor any of its employees are an employee or agent for Telstra. Telstra is not liable for any damage or loss caused by the Certified Locating Organisation or its employees.

Once all work is completed, the excavation should be reinstated with the same type of excavated material unless specified by Telstra.

The information contained within this pamphlet must be used in conjunction with other material supplied as part of this request for information to adequately control the risk of potential asset damage.

When using excavators and other machinery, also check the location of overhead power lines.

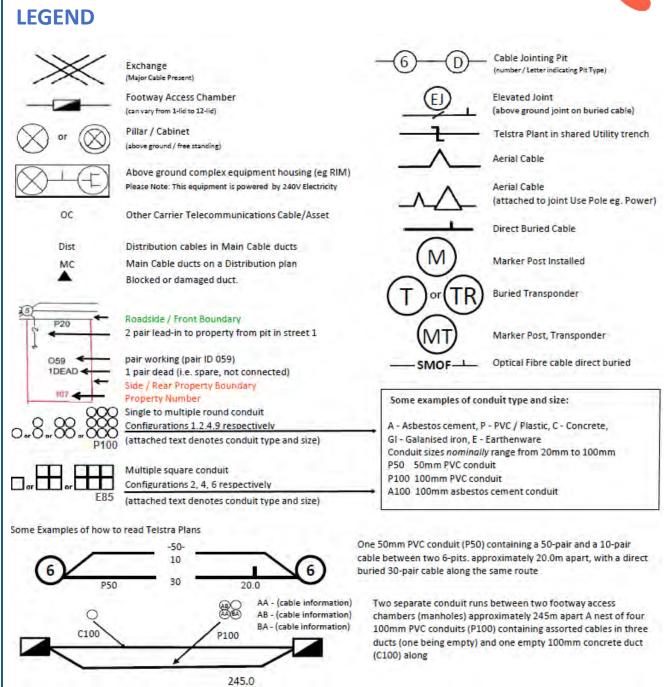
Workers and equipment must maintain safety exclusion zones around power lines

WARNING: Telstra plans and location information conform to Quality Level 'D' of the Australian Standard AS 5488 - Classification of Subsurface Utility Information. As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D. Refer to AS 5488 for further details. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy shown on the plans. FURTHER ON SITE INVESTIGATION IS REQUIRED TO VALIDATE THE EXACT LOCATION OF TELSTRA PLANT PRIOR TO COMMENCING CONSTRUCTION WORK. A plant location service is an essential part of the process to validate the exact location of Telstra assets and to ensure the assets are protected during construction works. The exact position of Telstra assets can only be validated by physically exposing them. Telstra will seek compensation for damages caused to its property and losses caused to Telstra and its customers.

Privacy Note

Your information has been provided to Telstra by BYDA to enable Telstra to respond to your BYDA request. Telstra keeps your information in accordance with its privacy statement. You can obtain a copy at www.telstra.com.au/privacy or by calling us at 1800 039 059 (business hours only).





Protect our Network:

by maintaining the following distances from our assets:

- 1.0m Mechanical Excavators, Farm Ploughing, Tree Removal
- 500mmVibrating Plate or Wacker Packer Compactor
- 600mm Heavy Vehicle Traffic (over 3 tonnes) not to be driven across Telstra ducts or plant.
- 1.0mJackhammers/Pneumatic Breakers
- 2.0m Boring Equipment (in-line, horizontal and vertical)

For more info contact a <u>CERTLOC Certified Locating Organisation (CLO)</u> or Telstra Location Intelligence Team 1800 653 935



Appendix E

Terrestrial Biodiversity Map





Subject Site Biodiversity Overlay **LOCALITY PLAN**Biodiversity Sensitivity - Terrestrial Biodiversity

5721B Sturt Highway MONAK

for Marciano Table Grapes







Appendix F

Riparian Land and Watercourses Map



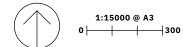


Subject Site Biodiversity Overlay

LOCALITY PLAN Riparian Land/Watercourse

5721B Sturt Highway MONAK

for Marciano Table Grapes







Appendix GWetlands Map





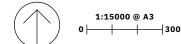
Subject Site
Wetland Overlay

LOCALITY PLAN Wetlands

vvettaria

5721B Sturt Highway MONAK

for Marciano Table Grapes

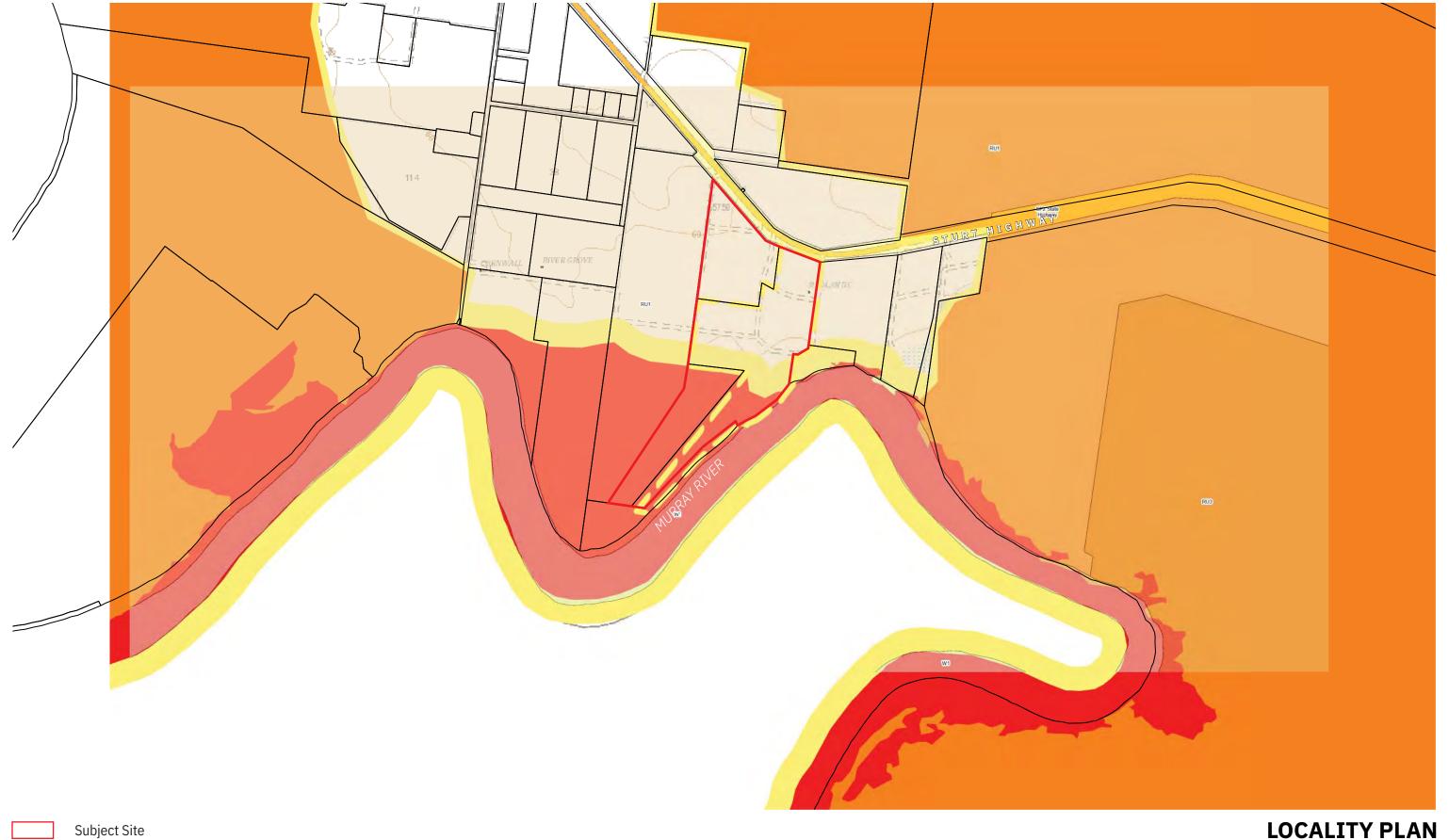






Appendix HBushfire Prone Land Map

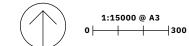




LOCALITY PLAN Bushfire Prone Area

5721B Sturt Highway MONAK

for Marciano Table Grapes



Vegetation Category 1

Vegetation Category 2

Vegetation Category 3

Vegetation Buffer





Appendix IAIHMS Search Results



Your Ref/PO Number : 20071

Client Service ID: 1018155

Date: 27 June 2025

Masterplan Consultants

tba tba

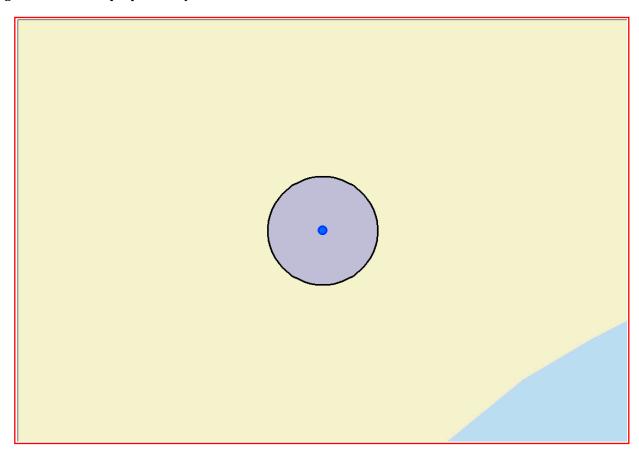
Attention: Jasmine Walters

Email: jasminew@masterplan.com.au

Dear Sir or Madam:

AHIMS Web Service search for the following area at Address: 5721B STURT HIGHWAY MONAK 2738 with a Buffer of 50 meters, conducted by Jasmine Walters on 27 June 2025.

The context area of your search is shown in the map below. Please note that the map does not accurately display the exact boundaries of the search as defined in the paragraph above. The map is to be used for general reference purposes only.



A search of Heritage NSW AHIMS Web Services (Aboriginal Heritage Information Management System) has shown that:

0	Aboriginal sites are recorded in or near the above location.
0	Aboriginal places have been declared in or near the above location. *

If your search shows Aboriginal sites or places what should you do?

- You must do an extensive search if AHIMS has shown that there are Aboriginal sites or places recorded in the search area.
- If you are checking AHIMS as a part of your due diligence, refer to the next steps of the Due Diligence Code of practice.
- You can get further information about Aboriginal places by looking at the gazettal notice that declared it. Aboriginal places gazetted after 2001 are available on the NSW Government Gazette (https://www.legislation.nsw.gov.au/gazette) website. Gazettal notices published prior to 2001 can be obtained from Heritage NSW upon request

Important information about your AHIMS search

- The information derived from the AHIMS search is only to be used for the purpose for which it was requested. It is not be made available to the public.
- AHIMS records information about Aboriginal sites that have been provided to Heritage NSW and Aboriginal places that have been declared by the Minister;
- Information recorded on AHIMS may vary in its accuracy and may not be up to date. Location details are recorded as grid references and it is important to note that there may be errors or omissions in these recordings,
- Some parts of New South Wales have not been investigated in detail and there may be fewer records of Aboriginal sites in those areas. These areas may contain Aboriginal sites which are not recorded on AHIMS.
- Aboriginal objects are protected under the National Parks and Wildlife Act 1974 even if they are not recorded as a site on AHIMS.

ABN 34 945 244 274

Email: ahims@environment.nsw.gov.au

Web: www.heritage.nsw.gov.au

• This search can form part of your due diligence and remains valid for 12 months.

Your Ref/PO Number : 20071

Client Service ID : 1040817

Date: 04 September 2025

Masterplan Consultants

tba tba

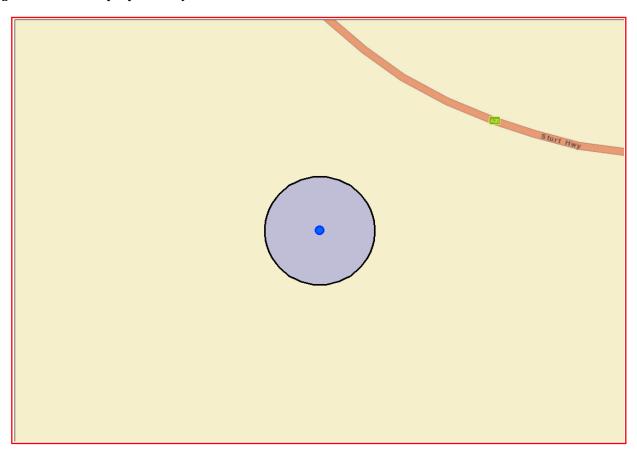
Attention: Jasmine Walters

Email: jasminew@masterplan.com.au

Dear Sir or Madam:

AHIMS Web Service search for the following area at Address: 5758 STURT HIGHWAY MONAK 2738 with a Buffer of 50 meters, conducted by Jasmine Walters on 04 September 2025.

The context area of your search is shown in the map below. Please note that the map does not accurately display the exact boundaries of the search as defined in the paragraph above. The map is to be used for general reference purposes only.



A search of Heritage NSW AHIMS Web Services (Aboriginal Heritage Information Management System) has shown that:

0	Aboriginal sites are recorded in or near the above location.
0	Aboriginal places have been declared in or near the above location.*

If your search shows Aboriginal sites or places what should you do?

- You must do an extensive search if AHIMS has shown that there are Aboriginal sites or places recorded in the search area.
- If you are checking AHIMS as a part of your due diligence, refer to the next steps of the Due Diligence Code of practice.
- You can get further information about Aboriginal places by looking at the gazettal notice that declared it. Aboriginal places gazetted after 2001 are available on the NSW Government Gazette (https://www.legislation.nsw.gov.au/gazette) website. Gazettal notices published prior to 2001 can be obtained from Heritage NSW upon request

Important information about your AHIMS search

- The information derived from the AHIMS search is only to be used for the purpose for which it was requested. It is not be made available to the public.
- AHIMS records information about Aboriginal sites that have been provided to Heritage NSW and Aboriginal places that have been declared by the Minister;
- Information recorded on AHIMS may vary in its accuracy and may not be up to date. Location details are recorded as grid references and it is important to note that there may be errors or omissions in these recordings,
- Some parts of New South Wales have not been investigated in detail and there may be fewer records of Aboriginal sites in those areas. These areas may contain Aboriginal sites which are not recorded on AHIMS.
- Aboriginal objects are protected under the National Parks and Wildlife Act 1974 even if they are not recorded as a site on AHIMS.

ABN 34 945 244 274

Email: ahims@environment.nsw.gov.au

Web: www.heritage.nsw.gov.au

• This search can form part of your due diligence and remains valid for 12 months.



Appendix J

NSW Planning Portal – Property Report





5721B STURT HIGHWAY MONAK 2738



Property Details

Address: 5721B STURT HIGHWAY MONAK 2738

Lot/Section 2/-/DP1248259

/Plan No:

Council: WENTWORTH SHIRE COUNCIL

Summary of planning controls

Planning controls held within the Planning Database are summarised below. The property may be affected by additional planning controls not outlined in this report. Please contact your council for more information.

Local Environmental Plans Wentworth Local Environmental Plan 2011 (pub. 16-12-2011)

Land Zoning RU1 - Primary Production: (pub. 21-4-2023)

Height Of Building NA Floor Space Ratio NA

Minimum Lot Size 10000 ha

Heritage NA
Land Reservation Acquisition NA
Foreshore Building Line NA

Riparian Lands and Watercourses Watercourse

Terrestrial Biodiversity Terrestrial Biodiversity

Wetlands Wetlands

Detailed planning information

State Environmental Planning Policies which apply to this property

State Environmental Planning Policies can specify planning controls for certain areas and/or types of development. They can also identify the development assessment system that applies and the type of environmental assessment that is required.



5721B STURT HIGHWAY MONAK 2738

- State Environmental Planning Policy (Biodiversity and Conservation) 2021: Excluded (pub. 21 -10-2022)
- State Environmental Planning Policy (Biodiversity and Conservation) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Exempt and Complying Development Codes) 2008: Land Application (pub. 12-12-2008)
- State Environmental Planning Policy (Housing) 2021: Land Application (pub. 26-11-2021)
- State Environmental Planning Policy (Industry and Employment) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Planning Systems) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Primary Production) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Resilience and Hazards) 2021: Land Application (pub. 2

 12-2021)
- State Environmental Planning Policy (Resources and Energy) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Sustainable Buildings) 2022: Land Application (pub. 29-8-2022)
- State Environmental Planning Policy (Transport and Infrastructure) 2021: Land Application (pub. 2-12-2021)

Other matters affecting the property

Information held in the Planning Database about other matters affecting the property appears below. The property may also be affected by additional planning controls not outlined in this report. Please speak to your council for more information

1.5 m Buffer around Classified Classified Road Adjacent

Roads

Biodiversity Value (BV) Map Clearing native vegetation for a development on an area on the

BV Map may require a Biodiversity Development Assessment

Report. Consult your local council.

Bushfire Prone Land Vegetation Buffer

Vegetation Category

Land near Electrical Infrastructure This property may be located near electrical infrastructure and

could be subject to requirements listed under Transport and

Infrastructure SEPP 2021 Clause 2.48. Please contact

Essential Energy for more information.

Local Aboriginal Land Council DARETON
Regional Plan Boundary Far West

This report provides general information only and does not replace a Section 10.7 Certificate (formerly Section 149)



5758 STURT HIGHWAY MONAK 2738



Property Details

Address: 5758 STURT HIGHWAY MONAK 2738

Lot/Section 1/-/DP1248259 2/-/DP827371

/Plan No:

Council: WENTWORTH SHIRE COUNCIL

Summary of planning controls

Planning controls held within the Planning Database are summarised below. The property may be affected by additional planning controls not outlined in this report. Please contact your council for more information.

Local Environmental Plans Wentworth Local Environmental Plan 2011 (pub. 16-12-2011)

Land Zoning RU1 - Primary Production: (pub. 21-4-2023)

Height Of Building NA Floor Space Ratio NA

Minimum Lot Size 10000 ha

Heritage NA
Land Reservation Acquisition NA
Foreshore Building Line NA

Terrestrial Biodiversity Terrestrial Biodiversity

Wetlands Wetlands

Detailed planning information

State Environmental Planning Policies which apply to this property

State Environmental Planning Policies can specify planning controls for certain areas and/or types of development. They can also identify the development assessment system that applies and the type of environmental assessment that is required.



5758 STURT HIGHWAY MONAK 2738

- State Environmental Planning Policy (Biodiversity and Conservation) 2021: Excluded (pub. 21 -10-2022)
- State Environmental Planning Policy (Biodiversity and Conservation) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Exempt and Complying Development Codes) 2008: Land Application (pub. 12-12-2008)
- State Environmental Planning Policy (Housing) 2021: Land Application (pub. 26-11-2021)
- State Environmental Planning Policy (Industry and Employment) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Planning Systems) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Primary Production) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Resilience and Hazards) 2021: Land Application (pub. 2 -12-2021)
- State Environmental Planning Policy (Resources and Energy) 2021: Land Application (pub. 2-12-2021)
- State Environmental Planning Policy (Sustainable Buildings) 2022: Land Application (pub. 29-8-2022)
- State Environmental Planning Policy (Transport and Infrastructure) 2021: Land Application (pub. 2-12-2021)

Other matters affecting the property

Information held in the Planning Database about other matters affecting the property appears below. The property may also be affected by additional planning controls not outlined in this report. Please speak to your council for more information

1.5 m Buffer around Classified Classified Road Adjacent

Roads

Bushfire Prone Land Vegetation Buffer

Vegetation Category

Land near Electrical Infrastructure This property may be located near electrical infrastructure and

could be subject to requirements listed under Transport and

Infrastructure SEPP 2021 Clause 2.48. Please contact

Essential Energy for more information.

Local Aboriginal Land Council DARETON
Regional Plan Boundary Far West



Appendix KSEPP Assessment





SEPP Assessment

A comprehensive assessment of the proposed development against the relevant State Environmental Planning Policies (SEPP's)is provided in Tables K.1 to K.6. The assessment takes into consideration the relevant objectives and applicable development standards that are contained in the SEPP's.

State Environmental Planning Policy (Biodiversity and Conservation) 2021

Table K.1 – 3.6 Is the land potential koala habitat?

	PROVISION	ASSESSMENT
(1)	Before a council may grant consent to a development application for consent to carry out development on land to which this Part applies, the council must be satisfied as to whether or not the land is a potential koala habitat.	□ Complies For the following reasons:
(2)	The council may be satisfied as to whether or not land is a potential koala habitat only on information obtained by it, or by the applicant, from a person who is qualified and experienced in tree identification.	 The subject land has been used for agriculture for a number of years. On-site trees are typically arranged in clusters directly adjacent dwellings or around the site boundaries.
(3)	If the council is satisfied— (a) that the land is not a potential koala habitat, it is not prevented, because of this	The proposed structures will be sited over existing agricultural land and will not require the removal of vegetation.
	Chapter, from granting consent to the development application, or (b) that the land is a potential koala habitat, it must comply with section 3.7.	The subject land has not been identified as koala habitat by the State Government's ePlanning Spatial overlays.

Table K.2 – 3.7 Is the land core koala habitat?

	PROVISION	ASSESSMENT
(1)	Before a council may grant consent to a development application for consent to carry out development on land to which this Part applies that it is satisfied is a potential koala habitat, it must satisfy itself as to whether or not the land is a core koala habitat. The council may be satisfied as to whether or not land is a core koala habitat only on information obtained by it, or by the applicant, from a person with appropriate qualifications	 ☑ Complies For the following reasons: The subject land has not been identified as a core koala habitat by the State Government's ePlanning Spatial overlays.
<i>(</i> -)	and experience in biological science and fauna survey and management.	
(3)	 If the council is satisfied— (a) that the land is not a core koala habitat, it is not prevented, because of this Chapter, from granting consent to the development application, or (b) that the land is a core koala habitat, it must comply with section 3.8. 	



State Environmental Planning Policy (Exempt and Complying Development Codes) 2008

Table K.3 – Subdivision 15 Earthworks, retaining walls and structural support, 2.29 Specified development

PROVISION	ASSESSMENT
Earthworks and the construction or installation of a retaining wall or other form of structural support is development specified for this code if it is not carried out, constructed or installed on or in a heritage item or a draft heritage item, on a flood control lot or in an environmentally sensitive area.	 ☑ Complies For the following reasons: The proposed development will not be undertaken on a (or draft) heritage item. The subject land is not affected by flooding. The subject land is not identified as an environmentally sensitive area.

Table K.4 – Subdivision 15 Earthworks, retaining walls and structural support, 2.30 Development Standards

PROVISION	ASSESSMENT
The standards specified for that development are that the development must— (a) not be a cut or fill of more than 600mm below or above ground level (existing), and (b) be located at least 1m from each lot boundary, and (c) if it is carried out, constructed or installed in a heritage conservation area or a draft heritage conservation area—be located in the rear yard, and (d) be located at least 40m from a waterbody (natural), and (e) not redirect the flow of any surface water or ground water or cause sediment to be transported onto an adjoining property, and (f) if it is a retaining wall or structural support for excavation or fill, or a combination of both— (i) be not be more than 600mm high, measured vertically from the base of the development to its uppermost portion, and (ii) be separated from any retaining wall or other structural support on the site by at least 2m, measured horizontally, and (iii) be located at least 1m from any registered easement, sewer main or water main, and (iv) have adequate drainage lines connected to the existing stormwater drainage system for the site, and (g) if the fill is more than 150mm deep—not occupy more than 25% of the area of the lot, and	 ✓ Does not Comply For the following reasons: The proposed development will not be located at least 1m from the northern site boundary. Proposed HPN 1 will be located 0.5m from the northern site boundary, this is to allow for adequate coverage of the existing vineyards. Whilst the net will be setback approximately 5m from the northern boundary, the support posts and anchors will be located within 0.5m. Notwithstanding, the northern site boundary lies directly adjacent Sturt Highway and is separated from the road by a road reserve of approximately 16 metres. The proposed structure will not adversely impact upon the functionality of the road or road reserve and will be contained wholly within the site boundaries.



(h) if the fill is imported to the site—be free of building and other demolition waste, and only contain virgin excavated natural material (VENM) as defined in Part 3 of Schedule 1 to the Protection of the Environment Operations Act 1997, and (i) if the land is in a rural or conservation zone—not be fill of more than 100 cubic metres on each lot. Note— It is an offence to transport waste to a place other than an appropriate and lawful waste facility (see section 143 of the Protection of the Environment Operations Act 1997).

Table K.5 – Subdivision 16 Farm Buildings (other than stock holding yards, grain silos and grain bunkers), 2.31 Specified development

PROVISION	ASSESSMENT
The construction or installation of a farm building (other than a stock holding yard, grain silo or	

grain bunker) that is not used for habitable purposes is development specified for this code if it is—

- (a) constructed or installed on land in Zone RU1, RU2, RU3, RU4 or RU6, and
- not constructed or installed on or in a heritage item or a draft heritage item or in an environmentally sensitive area, and
- (c) not constructed or installed on land shown on any relevant Procedures for Air Navigation Services—Aircraft Operations Map prepared by the operator of an aerodrome or airport operating within 2 kilometres of the proposed development and for which a PANS-OPS surface is identified that may compromise the effective and on-going operation of the relevant aerodrome or airport.

Note 1-

Farm building is defined in the Standard Instrument as a structure the use of which is ancillary to an agricultural use of the landholding on which it is situated and includes a hay shed, stock holding yard, machinery shed, shearing shed, silo, storage tank, outbuilding or the like, but does not include a dwelling.

Note 2-

Subdivisions 16A and 16B make special provision for farm buildings that are stock holding yards, grain silos or grain bunkers.

For the following reasons:

- The proposed development meets the criteria for a 'farm building' as defined in Note 1 of clause 2.31.
- The proposed development will not be installed on or in a draft heritage item or in an environmentally sensitive area.
- The proposed development will not be constructed or install on land shown on any relevant Procedures for Air Navigation Services – Aircraft Operations Map of an aerodrome or airport operating within 2km of the Site.



Table K.6 – Subdivision 16 Farm Buildings (other than stock holding yards, grain silos and grain bunkers), 2.32 Development Standards

PROVISION	ASSESSMENT
FROVISION	ASSESSMENT

- (1) The following standards are specified for that development—
 - (a) the development must not be higher than—
 - (i) for a landholding that has an area of less than 10ha—7m above ground level (existing), and
 - (ii) for a landholding that has an area of 10ha or more—10m above ground level (existing).
 - (b) if the development is located on land that is identified for the purposes of an environmental planning instrument as "Land with scenic and landscape values" on a Scenic and Landscape Values Map or as "Scenic Protection Area" on a Scenic Protection Map or Scenic Protection Area Map—it must not be higher than 7m,
 - (c) if the development-
 - (i) is on a landholding that has an area of more than 4ha, and
 - (ii) is on a landholding in relation to which the natural ground at any point within 100m of the ridgeline of any hill is at least 20m lower than the ridgeline, and
 - (iii) is located within 100m of that ridgeline, it must be sited on the landholding so that the highest point of the development is at least 5m below that ridgeline,
 - (d) subject to paragraph (e), the footprint of a farm building must not exceed 200m2,
 - (e) the footprint of all farm buildings (other than grain bunkers) on a landholding must not exceed the footprint shown in the following table—

exceed the real print energy in the real exceeding teacte		
Landholding area	Maximum footprint of all farm buildings (other	
0-4ha	than grain bunkers)	
>4ha-10ha	2.5% of the area of the landholding	
>10ha	1,000m2	
	2,000m2	

(f) the development must be located at least 20m from any road boundary and have a minimum setback from any other boundary as shown in the table to this paragraph—

Building footprint	Minimum setback from boundary
0-100m2	10m
>100m2-200m2	50m

□ Does not Comply

For the following reasons:

- The proposed farm buildings will exceed 2,000m² both individually and cumulatively.
- HPN 3 will be located within 20m of the road boundary.
- Each of the farm buildings will be located within 50m of the site boundaries.
- Proposed farm building B will adjoin the existing HPN structure.
- The proposed farm buildings will adjoin each other and thereby not achieve a 6 metre separation from other farm buildings
- The proposed hail proof netting structures will be contained entirely within the site boundaries with minimal impact on the surrounding environment. The structures do not incorporate solid walls and thereby provide some transparency to the land internal to and external of the structures. The proposed structures do not prejudice the land for its primary purpose being primary production and instead supporting ongoing use of the land for agricultural purposes, namely the growing of table grapes. The netting structures seek only to protect existing vineyards from undue weather events.



PROVISION ASSESSMENT

- a farm building must be located at least 6m from any other farm building (including any farm building that is a stock holding yard, grain silo or grain bunker) on the landholding or on an adjoining landholding,
- (h) the development must be located at least 50m from a waterbody (natural),
- the development must be designed by, and constructed in accordance with the specifications of, a professional engineer,
- (j) if the development is a shipping container, there must not be more than the following number of shipping containers per landholding—
 - (i) for a landholding that has an area of less than 400ha—1,
 - (ii) for a landholding that has an area of 400ha or more—5,
- (k) the development must not penetrate any obstacle limitation surface shown on any relevant Obstacle Limitation Surface Plan that has been prepared by the operator of an aerodrome or airport operating within 2 kilometres of the proposed development and reported to the Civil Aviation Safety Authority,
- (l) despite clause 2.30(a), excavation for the purposes of structural supports may exceed a depth of 600mm, measured from ground level (existing), unless the land is identified for the purposes of an environmental planning instrument as Class 1–5 on an Acid Sulfate Soils Map.
- (2) In this clause, footprint means the area of the ground surface occupied by a building, including the walls, footings and roofing of the building, and extending to the perimeter of the foundations and other means of structural support to the building, but does not include the area of access ramps, eaves and sunshade devices.

Note 1-

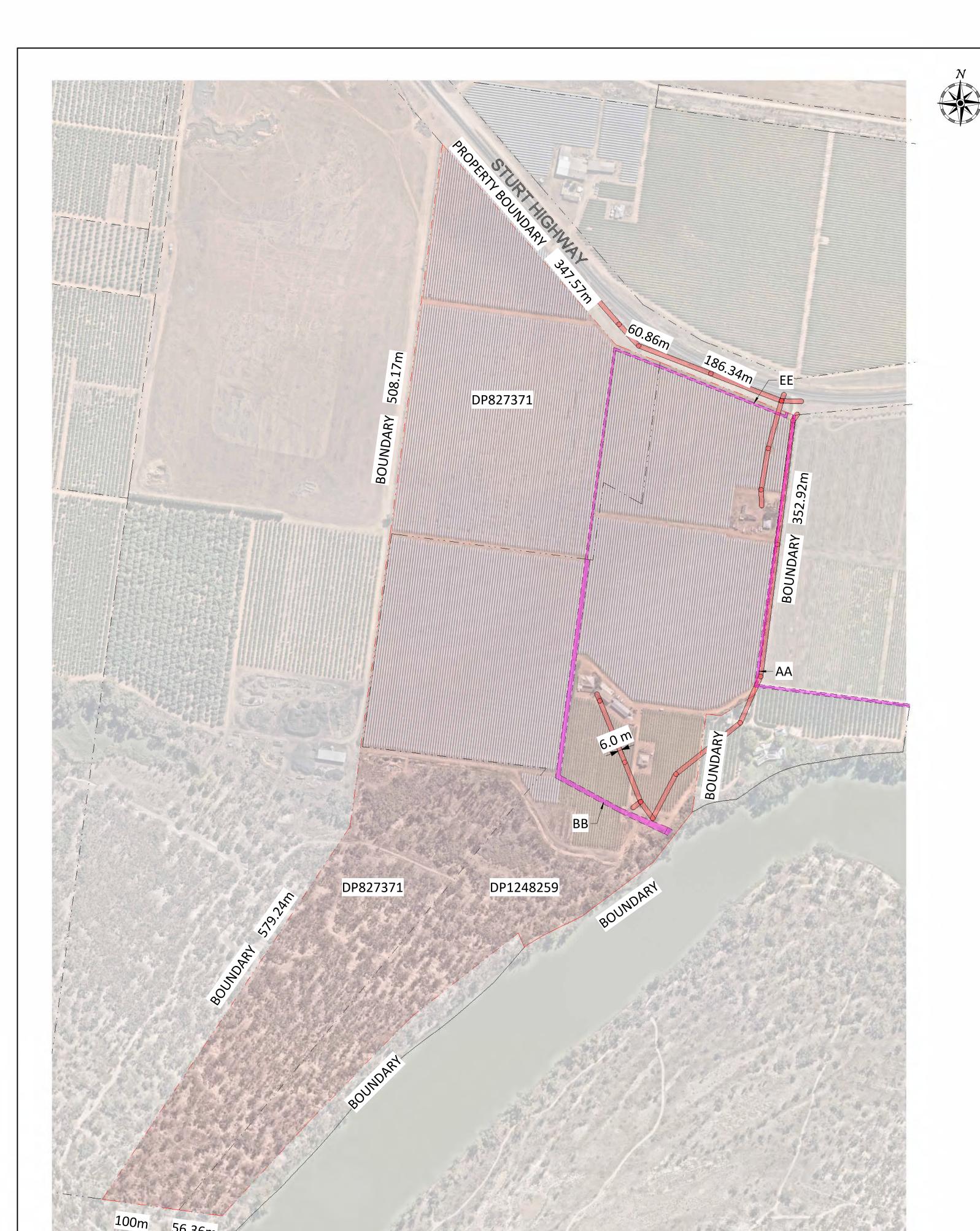
There are other existing legislative requirements relating to the clearance of power lines, substations and Obstacle Limitation Surfaces near airport flight paths.

Note 2-

The consent of the appropriate roads authority is required under section 138 of the Roads Act 1993 for the carrying out of certain works in relation to roads, including the building of any crossover or creating road access.







DA - Existing Site Plan

1:3000

1:3000 Scale Bar

STRUCTURE LEGEND STRUCTURE HEIGHT: 5.0 METRES SITE BOUNDARY **EASEMENTS** POWER LINE CLEARANCE

No.	Revision Information	Ву	Date

Structure Height

Flat Top Structure Height (H)

THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Project Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

Drawing Title **EXISTING SITE PLAN**

Client Name:

P&T Marciano Scale @ A1 As indicated Checked

HH JG2
Project No. Sheet No. Rev.

1759 - 101 - .



STRUCTURE LEGEND

STRUCTURE HEIGHT:

5.0 METRES

TOP NETTING TYPE:

Construction: Lock stitch knitted HDPE monofilament

20mm Hexagonal hole with cross over

Weight of Net: 75 grams/mtr

Nominal shade factor: 12%



SITE BOUNDARY

EASEMENTS

POWER LINE CLEARANCE

PROPOSED NETTING STRUCTURE

ANCHOR LINE

THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Project Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

No. Revision Information

Flat Top Structure Height (H)

Structure Height

Drawing Title PROPOSED SITE PLAN

Client Name:

P&T Marciano Scale @ A1 As indicated

Checked

HH JG2
Project No. Sheet No. Rev.

1759 - 102 - .

214.4 m 239.6 m

Site - Plan (Sales)

1:1000

Drawing Approvals

These drawings have been reviewed by the client and approved for installation. Any variation, alteration, change or modification to the design and/or materials, following this approval, must be in writing and signed by the client or their authorised representative, and the company reserves the right to vary the quotation accordingly.

approval, must be in writing and signed by the client or their authorised represent the company reserves the right to vary the quotation accordingly.

Signed:

Position:

Company:

FOR APPROVAL

No. Revision Information By Date

-- First Issue 28Mar25

Sheet List - Sales

Drawing Sheet Name

1759-001 SITE PLAN

1759-002 DETAIL SHEET 01

Structure Height

Flat Top Structure Height (H)

Top Net
Ref G2 Code Description

1616 QNW161630 16mm 16x300m White Quad Crossover

2020 QNW202030 20mm 20x300m White (

Structure Site Legend

Posts
IP PP PPA CP/PBP IBP GA Typi

Wire and Cable

Double Cable / Wire
7.5mm Cable
6mm Cable
3.15mm Wire High Tensile
3.15mm Spring Wire
2.65mm Wire High Tensile

Line Types

Site Boundary

Easement Locations

Overhead Powerlines - Low Voltage
Overhead Powerlines - High Voltage
Fence Line

UNLESS OTHERWISE STATED: LINEAR TOLERANCE ± 0.5m, ANGULAR TOLERANCE ± ANCHOR DISTANCE CAN ONLY BE INCREASE



THIS DRAWING IS FOR DESIGN GUIDANCE ONLY. FINAL DETAILS MUST MEET SITE CONDITIONS, THE REQUIREMENTS OF ALL RELEVANT AUTHORITIES, APPLICABLE AUSTRALIAN STANDARDS AND THE BUILDING CODE OF AUSTRALIA. THE CONTRACTOR MUST VERIFY ALL DIMENSIONS ON SITE BEFORE COMMENCING ANY WORK OR MAKING SHOP DRAWINGS. FIGURED DIMENSIONS ARE NOT TO BE USED, SCALED DIMENSIONS MUST BE CHECKED. DO NOT SCALE THIS DRAWING.

Project Monak - table grapes

Project Address 5721B Strut Hwy, Monak NSW 2738

Drawing Title

SITE PLAN

Client Name:

P&T Marciano

Scale @ A0

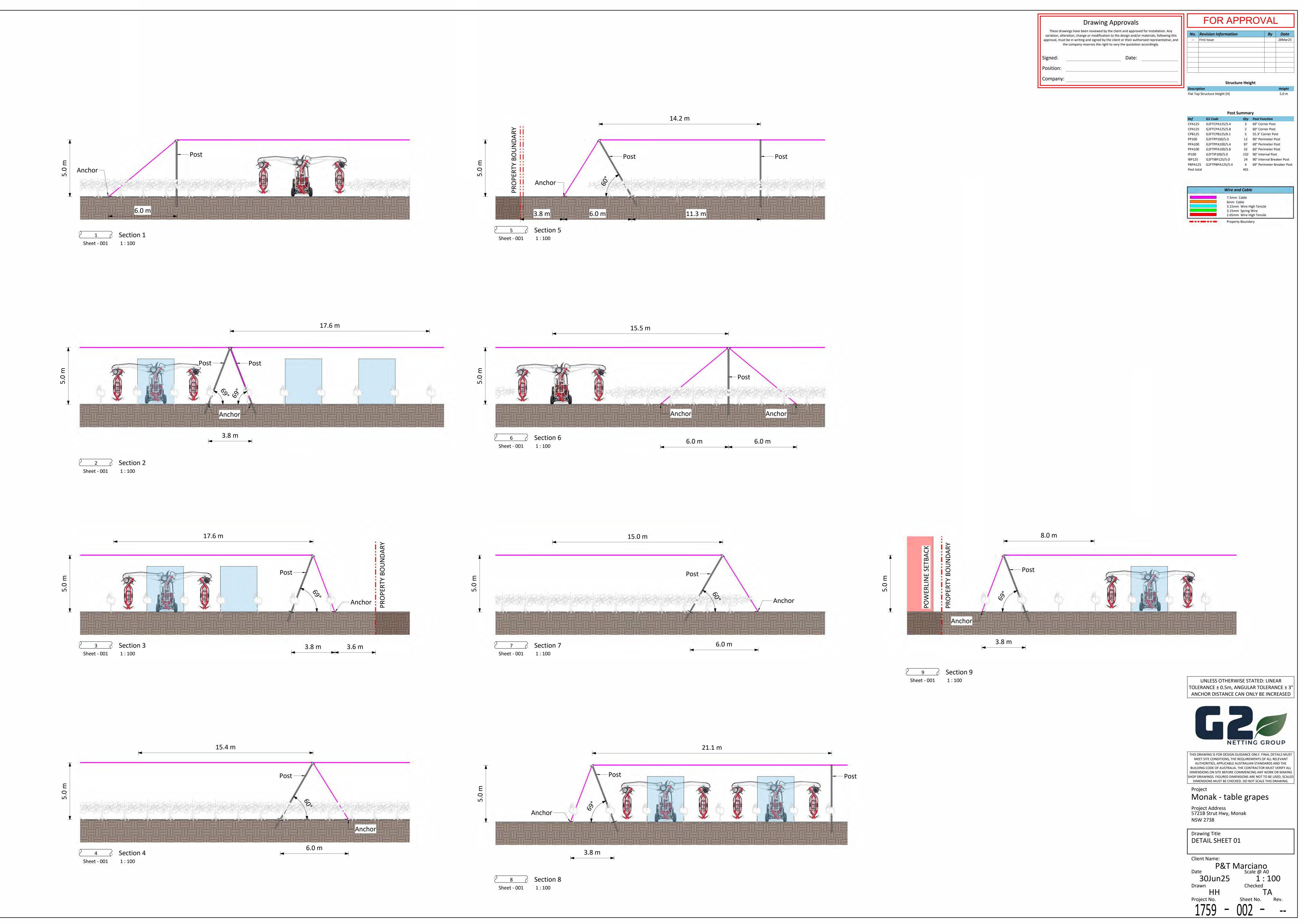
30Jun25 As indicate

Drawn Checked

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Project No.

1759 - 001 - --

Rev.



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